



UNIVERSIDAD PONTIFICIA COMILLAS  
ESCUELA TÉCNICA SUPERIOR DE INGENIERÍA (ICAI)

OFFICIAL MASTER'S DEGREE IN THE  
ELECTRIC POWER INDUSTRY

Master's Thesis

**MOTHBALLING MECHANISMS IN THE SPANISH  
POWER SYSTEM: ECONOMIC AND OPERATIONAL  
ASSESSMENT**

Author: Irene Campos Blanco  
Supervisor: Javier García González

Madrid, July 2015

## Master's Thesis Presentation Authorization

THE STUDENT:

Irene Campos Blanco

.....

THE SUPERVISOR

Dr. Javier García González

Signed: ..... Date: ...../ ...../ .....

THE CO-SUPERVISOR

Signed: ..... Date: ...../ ...../ .....

Authorization of the Master's Thesis Coordinator

Dr. Javier García González

Signed: ..... Date: ...../ ...../ .....



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## SUMMARY

During the last years, combined cycles have been significantly displaced from the Spanish market due to the lower demand and its higher coverage with renewable energy sources. Their production decline, combined with low wholesale electricity prices and higher operating costs than other generation technologies, have contributed to reduce the economic profitability of these facilities. As a result, the industry started to consider the convenience of closing (either permanently or temporarily) those power plants with low market share and not enough incomes to cover their operating expenses.

The electricity reform approved in 2013 establishes the regulatory framework to enable the mothballing of power plants in Spain, introducing the possibility of temporary closure of facilities and entitling the system operator to forecast the maximum capacity that may be withdrawn from the system, as well as to report on the need of reinstating mothballed power, when applicable.

The main objective of this thesis is to analyse what would be the economic and operational impacts derived from the introduction of power plant mothballing in the Spanish Power System, taking into account that the generation capacity could be adapted to the evolution of demand, thus, saving the costs associated with unnecessary plants being opened for commercial operation.

A midterm planning model, based in a centralised approach, is used to address the issue of generation planning, subject to ensure a desirable security of supply margin. The model provides a reference to determine what would be the expected outcome of mothballing in terms of decisions related to temporary closure and later restoring of facilities and their impact in the generation mix structure, operating costs and level of security of supply.

Three scenarios for the years 2015 and 2020 are defined in order to analyse the impact of mothballing in the Spanish Power System. The main results are 11.7 GW of mothballed power, reduction of operation costs in 379 M€ and lack of impact on the energy mix or CO<sub>2</sub> emissions in the year 2015. Additionally, the increase in demand considered for the scenario in 2020 do not reveal the need to reinstate mothballed power in the horizon 2015-2020.

## RESUMEN

Durante los últimos años, los ciclos combinados se han visto significativamente desplazados del mercado español debido a la menor demanda y su mayor cobertura con fuentes de energía renovables. La reducción de su producción, combinada con bajos precios del mercado eléctrico y mayores costes de operación que otras tecnologías de generación, han contribuido a reducir la rentabilidad económica de estas instalaciones. Como resultado, el sector empezó a considerar la conveniencia de cerrar (permanentemente o temporalmente) aquellas centrales con baja cuota de mercado y sin suficientes ingresos para cubrir sus gastos de operación.

La reforma eléctrica aprobada en 2013 establece el marco regulatorio para permitir la hibernación de centrales eléctricas en España, introduciendo la posibilidad del cierre temporal de instalaciones y habilitando al operador del sistema a estimar la capacidad que puede ser retirada del sistema, así como informar de la necesidad de reincorporar potencia hibernada, cuando sea aplicable.

El principal objetivo de esta tesis es analizar cuáles serían los impactos económicos y de operación derivados de la introducción de la hibernación de centrales en el Sistema Eléctrico Español, teniendo en cuenta que la capacidad de generación podría ser adaptada a la evolución de la demanda, evitando así los costes asociados a la operación comercial de las plantas que no sean necesarias.

Se ha utilizado un modelo de planificación a medio plazo, basado en una perspectiva centralizada, para abordar la planificación de generación, garantizando un margen de seguridad de suministro deseable. El modelo proporciona una referencia para determinar cuál sería el resultado esperado de la hibernación en términos de decisiones relacionadas con el cierre temporal y posterior reincorporación y su impacto en la estructura del mix de generación, los costes de operación y la seguridad de suministro.

Se han definido tres escenarios para los años 2015 y 2020 con el fin de analizar el impacto de la hibernación en el Sistema Eléctrico Español. Los principales resultados son 11.7 GW de potencia hibernada, reducción de los costes de operación en 379 M€ y ausencia de impacto en el mix de energía o las emisiones de CO<sub>2</sub> en el año 2015. Además, el incremento de demanda considerado para el escenario en 2020 no muestra la necesidad de reincorporar potencia hibernada en el horizonte 2015-2020.

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## 1 Introduction

### 1.1 Motivation and problem description

The current state of the Spanish power industry is defined to a great extent by the drop of electricity consumption, the large penetration of renewable generation and the reduced interconnection capacity with adjacent countries. This context, together with the excess of installed capacity, has revealed a lower involvement of some agents in the wholesale electricity market (especially those who operate the peak power plants).

This is the case of the combined cycle power plants, which have been significantly displaced from the Spanish market due to the lower demand and its higher coverage with renewable energy sources. As a consequence, these facilities have experienced an important reduction in operation hours and contribution to demand coverage, declining their share in the generation mix from 32% in 2008 to 8.5% in 2014.

The production decline described above, combined with low wholesale electricity prices and higher operating costs than other generation technologies, have contributed to reduce the economic profitability of the combined cycles. As a result, the industry started to consider the convenience of closing (either permanently or temporarily) those facilities with low market share and not enough incomes to cover their operating expenses.

In case that a power plant is permanently retired before its expected decommission date, the situation is irreversible: the owner would be unable to recover some of the investment costs and the system would face a permanent capacity withdrawal. On the other hand, the temporary shut-down of the facility (also called mothballing) could represent an alternative to the freedom of exit the market that may entail some benefit for both producers and consumers.

In other words, power plant mothballing may act as a mechanism to cope with the cyclical behaviour of power systems, providing market agents with some flexibility to adapt their generation portfolio to the projected demand. This means that capacity could be withdrawn from the system in periods of oversupply (allowing producers to save some operating costs) and it could be restored when market conditions are more favourable (and agents are able to recover their investments). Consumers, in turn, could benefit from the reduction of some regulated costs when there is overcapacity and plants do not need to be available, as well as from the rapid entry of de-mothballed capacity in periods of supply scarcity.

In this context, the electricity reform approved in 2013, the Act 24/2013 of the Power Sector, establishes the regulatory framework to enable the mothballing of power plants in Spain. The Act

introduces the possibility of temporary closure of facilities (subject to administrative authorisation) and entitles the system operator to forecast the maximum capacity that may be withdrawn from the system, as well as to report on the need of reinstating mothballed power, when applicable.

The aim of this master thesis is to assess the economical and operational effects of the introduction of power plant mothballing in the Spanish Power System. The main issue is to address the question of generation planning, subject to ensure a desirable security of supply margin, taking into account that the generation capacity could be adapted to the evolution of demand, thus, saving the costs associated with unnecessary plants being opened for commercial operation.

A centralised generation planning model is used to tackle the problem from the perspective of the system operator. This approach provides a reference to determine what would be the expected outcome of the implementation of mothballing mechanisms in the current Spanish System in terms of decisions related to temporary closure and later restoring of facilities and their impact in the generation mix structure, operating costs and level of security of supply.

The work presented in the thesis is supported by the analysis of different scenarios developed to explore the influence of mothballing on operational costs and generation structure.

## 1.2 Objectives

The main objective of this thesis is to analyse what would be the economic and operational impacts derived from the introduction of power plant mothballing in the Spanish Power System.

It is proposed a decision support model, based in a centralised generation planning approach, to accomplish this objective and to address the following questions:

- How much power should be mothballed considering the current state of the system?
- How would security of supply be affected?
- What technologies would replace the capacity withdrawal in the energy mix?
- What would be the impact on operating costs?
- How much should demand increase in order to reinstate mothballed plants?

### 1.3 Methodology

The objective of the master thesis is to assess the impact on costs and operation of the future implementation of mothballing mechanisms in Spain. The proposed methodology to perform this assessment is indicated below:

- Analysis of the current situation in the Spanish Power System:

The Spanish case is studied, looking at current market conditions which jeopardize the economic viability of combined cycles and examining the new regulation that allows their temporary closure.

- Development of decision support model:

The “Midterm planning model” studied during the course “Decision support models for the electric power industry” is adapted to incorporate mothballing decisions to the dynamics of generation planning. The proposed model considers such decisions based on the projected savings in operating costs and subject to ensure a sufficient level of security of supply.

The main features of the proposed model are:

- Centralised approach based on minimisation of operating costs from the system operator's perspective
- Medium term scope adopting a time horizon of one year
- Main assumptions: transmission grid is not modelled, system evolution is represented by load blocks instead of chronologically, single reservoirs are used to model the behaviour of all hydro units, uncertainty of input data is neglected
- Deterministic approach using estimated values of input data (demand, production of renewable energy sources, fuel costs, hydrology, etc.)
- Incorporation of fixed operating costs in the objective function
- Consideration of constraints related to security of supply and dispatchable capacity

During this stage, the thesis problem is conceptualised and formalised through the proposed model and the required input data is collected. The data is introduced in the model for its implementation, validation and use.

- Scenarios generation:

Three scenarios for the years 2015 and 2020 are selected to infer the evolution of mothballing decisions over time, as well as to analyse their impact on operation costs and scheduling.

## 2 An approach to the Spanish case

In this chapter, it is presented the case of mothballing in the Spanish System framework, introducing some considerations of the Spanish market, the situation of combined cycles and the related regulation.

### 2.1 Market considerations

The Spanish Power System has observed a decrease in electricity demand (see Figure 1) during the past years, mainly derived from the macroeconomic scenario of economic crisis that started in 2007.

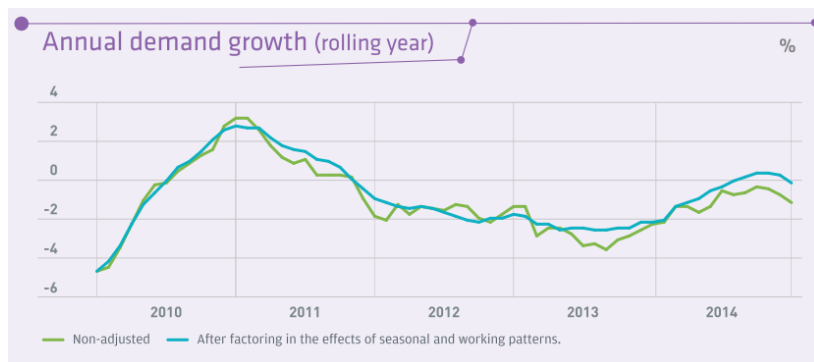


Figure 1: Evolution of electricity demand. Years 2010-2014 (Source REE)

The actual demand experienced during these last years was significantly below the values foreseen in the planning scenarios and, therefore, there are more generation facilities than the actual needs of the system.

Together with the drop in demand, it has been a progressive increase in integration of renewable resources (see Figure 2), that has also resulted in a market share reduction for other conventional generation technologies.

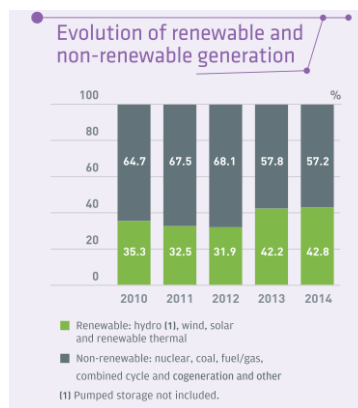


Figure 2: Evolution of renewable and non-renewable energy production. Years 2010-2014 (Source REE)



Additionally, the Spanish Power System has limited interconnection capacity with adjacent systems. Even though there are projects to increase the interconnection facilities (see Figure 3), they will not ensure significant energy exchanges with other markets.

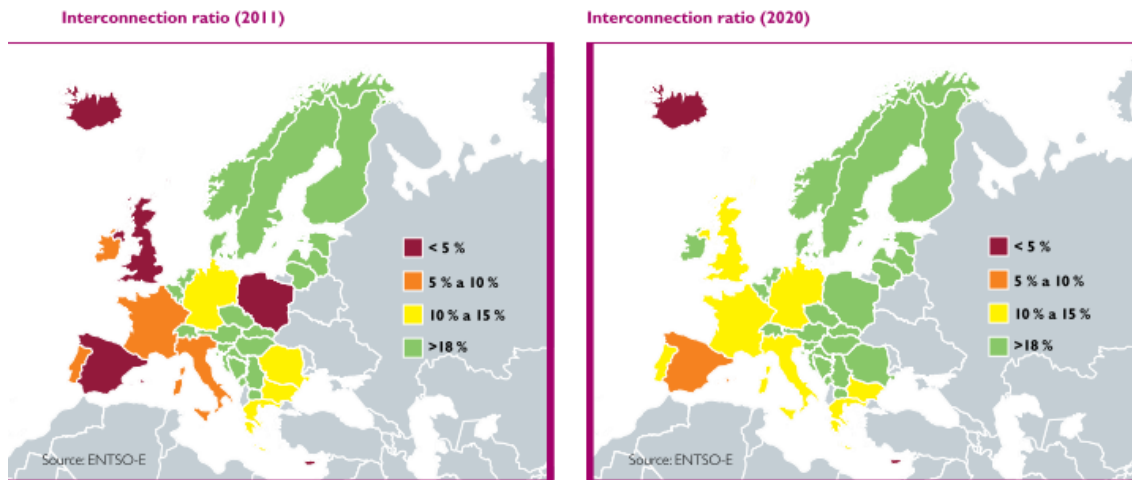


Figure 3: European interconnection ratios. Year 2011 and Year 2020 (Source ENTSO-E)

As a result of the drop in demand, the high level of renewable sources integration and the limited interconnection capacity, the current environment in the Spanish System is characterized by the overcapacity of installed power (see Figure 4).

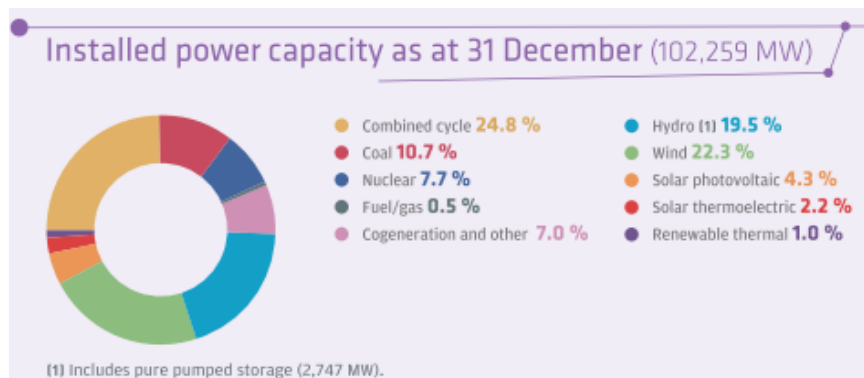


Figure 4: Installed power. Year 2014 (Source REE)

At the end of 2014, the installed capacity was around 102 GW, while the maximum peak demand was below 39 GW and the coverage index (relationship between the available power and the peak demanded) accounted for 1.4, which is significantly higher than the desirable coverage index (1.1).

In Figure 5 they are also included the coverage indexes for years 2007 to 2014, indicating an increasing evolution.

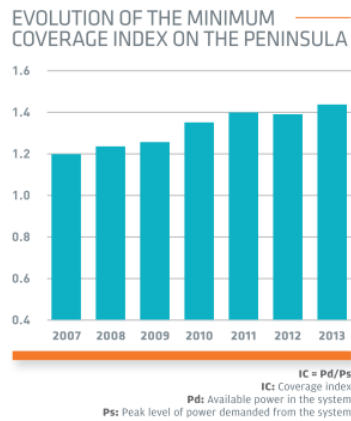


Figure 5: Evolution of coverage index. Years 2007-2013 (Source REE)

## 2.2 Current situation of combined cycles

As a result of the existing overcapacity some of the generation facilities are under-use, with the consequent negative impact in their economic profitability. This situation is amplified in the case of combined cycles where the evolution of fuel, electricity and CO<sub>2</sub> prices, as well as the regulations for domestic coal consumption, decrease even more their contribution to the energy mix.

See Figure 6 and Figure 7 where the evolution of the Spanish energy mix is represented, and Figure 8 that shows the changes in the spark spreads (margin between electricity and fuel price) for coal and gas.

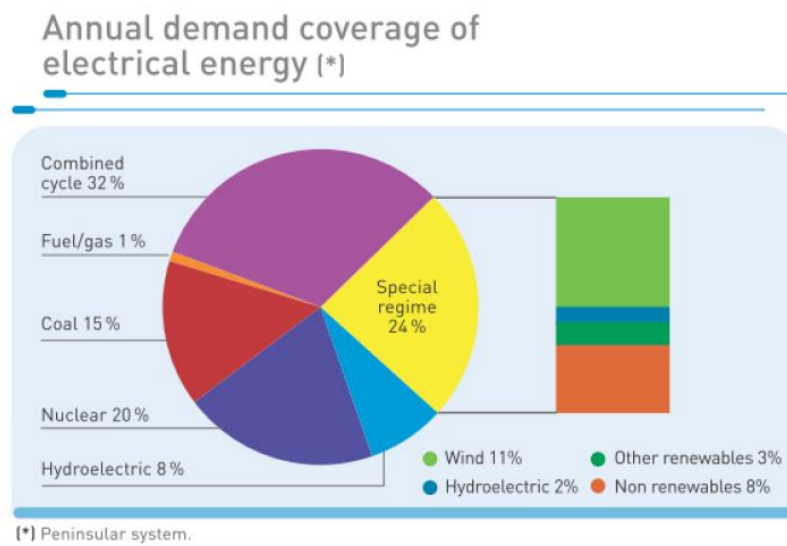


Figure 6: Energy mix. Year 2008 (Source REE)

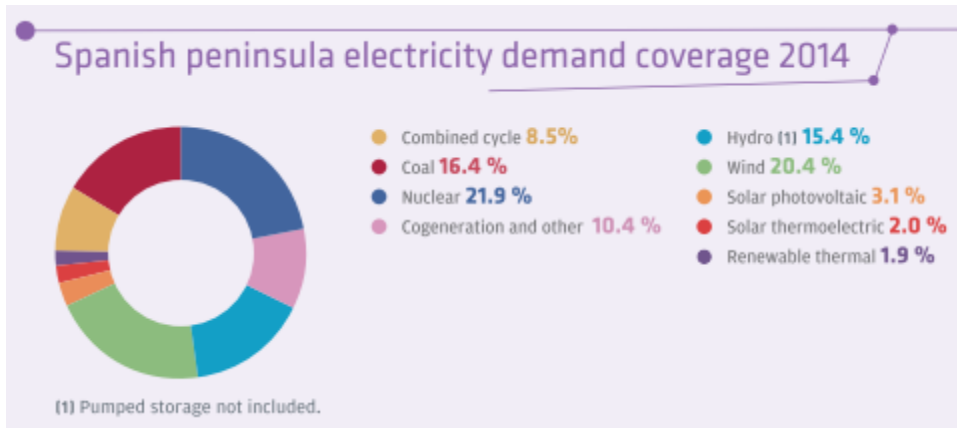


Figure 7: Energy mix. Year 2014 (Source REE)



Figure 8: Spark spreads for coal (during off-peak hours) and gas (during peak hours) in the German market (Source Platts from (Velázquez, 2014))

Consequently, the number of operation hours of the combined cycles is significantly curtailed (see Figure 9 below), accounting for less than 1000 hours in 2014 according to data reported by CNMC (CNMC, 2015).

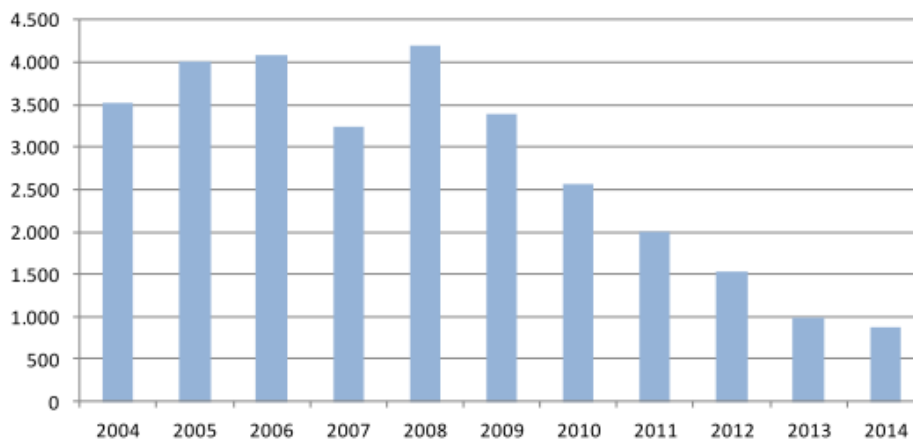


Figure 9: Evolution of equivalent operating hours at full load for combined cycles (Source CNMC)

The Spanish regulator has also indicated in its proposal for mechanisms for security of supply (CNE, 2012) that the overcapacity, together with the lack of mechanisms to exit the market, would have contributed to jeopardize the economic situation of combined cycles, with some of them unable to recover their fixed operating costs. See Figure 10 where the estimations from the CNMC are included.

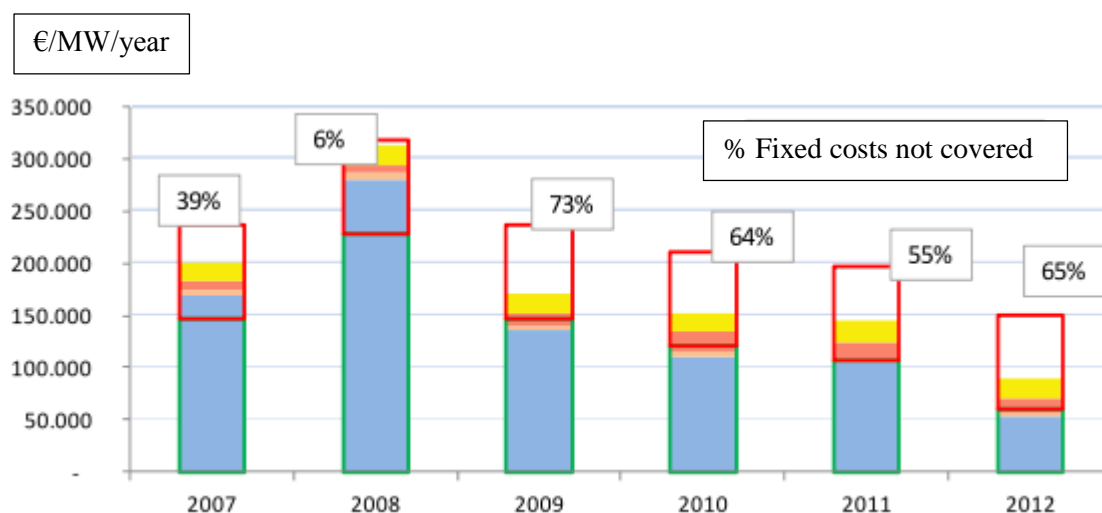


Figure 10: Evolution of non-recovery of fixed operating costs for combined cycles (Source CNMC)

### 2.3 The new regulatory framework

In this context, the Act 24/2013 of the Power Sector (BOE, 2013) enables the temporary closure of combined cycles (mothballing). The law establishes that the mothballing process will be subject to administrative authorisation and that the system operator will be entitled to forecast requirements for mothballing and power restoring.

The proposed mothballing mechanism is further developed on the Draft Royal Decree on capacity payments and mothballing (Secretaría de Estado de Energía, 2013). The relevant considerations for the aim of this thesis are indicated below:

- The mothballing mechanism would be allowed for combined cycles over 50 MW.
- The system operator would determine the amount of power to be mothballed (based on forecasts on security of supply, including evolution of coverage index, local/zonal constraints and any other issue relevant for security). Its forecasts would be based on scenarios with low hydraulicity and high demand.
- The mechanism included in the draft RD establishes the mothballing assignment through a decreasing auction for the power to be mothballed on the following year.

- The period for mothballing is established in one year (even though the first auction could be arranged for a longer period).
- Additionally, it is defined an incentive for dispatchable power, in order to recognise the value of available thermal power to face variations in demand and as back-up for renewable generation.
- The incentive for dispatchable power would be allowed for combined cycles and coal power plants, but not for hydropower or pumping stations. The requirements on dispatchable power for each year would be based on the maximum thermal gap occurred during the previous three years.

### 3 Generation planning model with mothballing. Application to the Spanish Power System

This chapter includes the characteristics of the model presented in the thesis, as well as the definition of the scenarios that are used to support the results and conclusions of this work.

It is considered a midterm temporal scope with time horizon of one year, in accordance with the regulatory proposals for mothballing mechanisms in Spain (refer to section 2.3). The temporal structure used in the model divides the yearly time horizon in periods (weeks), subperiods (working and non-working days) and load levels (five levels for working days and four levels for non-working days).

The proposed model is a midterm planning model based on a centralised approach and with mothballing decisions for combined cycles. The model is used to determine the optimal generation schedule over the considered time horizon (one year) and taking into account potential mothballing decisions for combined cycle units.

The mothballing decisions are incorporated in the model based on the projected savings in operating costs (introduction of fixed operating costs in the objective function) and subject to provide a sufficient level of security of supply (introduction of requirements for dispatchable generation in the model constraints).

Three scenarios are defined in order to analyse the impact on operation and costs derived from mothballing decisions, namely year 2015 without mothballing, year 2015 with mothballing and year 2020 with mothballing.

#### 3.1 Characteristics of the proposed model

##### 3.1.1 Formulation

The formulation of the optimization problem is presented below:

$$\begin{aligned}
 \text{Min} \quad & \sum_t \sum_p \sum_s \left\{ f_t \cdot \left[ \gamma_t \cdot y_{t,s,p} + \theta_t \cdot z_{t,s,p} + \sum_n a_{n,s,p} \cdot \left[ \alpha_t \cdot \frac{q_{t,n,s,p}}{k_t} + \beta_t \cdot u_{t,s,p} \right] \right] \right\} \\
 & + \sum_g \left\{ [o_g + pco2 \cdot emis_g] \cdot \sum_p \sum_s \sum_n \left[ a_{n,s,p} \cdot \frac{q_{g,n,s,p}}{k_g} \right] \right\} \\
 & + \sum_{gccgt} \text{foc} \cdot m_{gccgt} \cdot q_{gccgt}^{\max}
 \end{aligned} \tag{1}$$

s. t.

$$a_{n,s,p} \cdot \left[ \sum_t q_{t,n,s,p} + \sum_h (q_{h,n,s,p} - b_{h,n,s,p}) + \sum_{res} q_{res,n,s,p} \right] = a_{n,s,p} \cdot d_{n,s,p} \quad \forall n, s, p \quad (2)$$

$$q_{t,n,s,p} \leq u_{t,s,p} \cdot k_t \cdot q_t^{max} \quad \forall t, n, s, p \quad (3)$$

$$q_{h,n,s,p} \leq k_h \cdot q_h^{max} \quad \forall h, n, s, p \quad (4)$$

$$b_{h,n,s,p} \leq k_h \cdot b_h^{max} \quad \forall h, n, s, p \quad (5)$$

$$q_{t,n,s,p} \geq u_{t,s,p} \cdot k_t \cdot q_t^{min} \quad \forall t, n, s, p \quad (6)$$

$$q_{h,n,s,p} \geq q_h^{min} \quad \forall h, n, s, p \quad (7)$$

$$b_{h,n,s,p} \geq 0 \quad \forall h, n, s, p \quad (8)$$

$$w_{h,p} + \sum_{n,s} a_{n,s,p} (q_{h,n,s,p} - \eta_h b_{h,n,s,p}) \leq w_{h,p-1} + i_{h,p} \quad \forall h, p \quad (9)$$

$$w_{h,p} \leq w_{h,p}^{max} \quad \forall h, p \quad (10)$$

$$w_{h,p} \geq w_{h,p}^{min} \quad \forall h, p \quad (11)$$

$$q_{gccgt,n,s,p} \leq m_{gccgt} \cdot k_{gccgt} \cdot q_{gccgt}^{max} \quad \forall gccgt, n, s, p \quad (12)$$

$$\sum_{gccgt} u_{gccgt,s,p} \cdot k_{gccgt} \cdot q_{gccgt}^{max} + \sum_{gcg} u_{gcg,s,p} \cdot k_{gcg} \cdot q_{gcg}^{max} \geq thgap \quad \forall n, s, p \quad (13)$$

$$u_{t,lab,p} - u_{t,fes,p-1} = y_{t,lab,p} - z_{t,lab,p} \quad \forall t, p \quad (14)$$

$$u_{t,fes,p} - u_{t,lab,p} = y_{t,fes,p} - z_{t,fes,p} \quad \forall t, p \quad (15)$$

The objective of the problem is to determine the optimal generation schedule that minimises the objective function (1) in order to supply the electrical demand (2) and satisfy the technical constraints included in the model, (3)-(15), at minimum cost.

The proposed formulation incorporates the mothballing decisions as follows: on the one hand, fixed operating costs for combined cycles are included in the objective function (1), on the other hand, the available dispatchable generation is constrained to be able to cover the thermal gap required by the system (13).

Mothballing decisions will be made as long as the savings in fixed operating costs are greater than the variable costs incurred by the substitute technology, if any, and the available dispatchable generation is enough to satisfy the requirements of the system.

### 3.1.2 Input data

The set of input data used in the model is presented below, as well as the considerations followed to obtain the required information and to estimate the related parameters.

#### a) Generation units $g, t, h, res, gccgt, gcg$

The set of generators ( $g$ ) considered in the model is comprised by thermal generators ( $t$ ), hydraulic generators ( $h$ ) and renewable, cogeneration and waste-to-energy units ( $res$ ).

- Thermal generators include nuclear, coal, combined cycle and gas units installed in the Spanish Power System.
- Hydraulic generation is modelled through two aggregated reservoirs, one for hydraulic units connected to the hydro network and other for isolated units (closed-cycle pumped storage plants). Run-of-river plants are considered within the connected reservoir.
- Renewable generators comprise the following technologies: wind, solar photovoltaic, solar thermoelectric and renewable thermal (biogas and biomass). Each technology is represented in the model through an equivalent unit with the production associated to all generators of the aforementioned technology.
- Cogeneration and waste-to-energy units are also modelled with an equivalent unit with aggregated production.

Additionally, two subsets of generators are specifically defined to consider dispatchable generation such as combined cycle units ( $gccgt$ ) and coal/gas plants ( $gcg$ ) in the model.

The generation units are introduced in the model according to data available from REE (REE, 2014) and they are summarized in Annex A.

#### b) Generation mix and power limits for generation and pumping units $q_g^{max}, q_g^{min}, b_g^{max}$

The generation mix is defined in order to set the amount and type of generation available to meet demand in each scenario (refer to section 3.2).

Additionally, gross power limits (expressed in GW) are necessary to establish the feasible range for the operation of generation and pumping units:



- Maximum gross power for thermal generators is extracted from the information reported by REE (REE, 2014).
- Minimum gross power for thermal generators is estimated as 30% of the maximum gross power limit.
- Maximum gross power for hydraulic units connected to the hydro network is limited below the installed power due to physical constrains (turbines cannot operate all simultaneously at maximum capacity in order to avoid floods downstream). Therefore, the maximum limit for hydraulic generation in the connected reservoir is established as 10 GW according to data for maximum hydraulic production in 2014 (REE, 2015b).
- Since run-of-river plants are modelled within the connected reservoir, average production of these plants may be used to determine the minimum gross power for hydraulic generation in the aforementioned reservoir. According to data of run-of-river production in 2014 (REE, 2015b), 0.4 GW is considered as the minimum gross power for hydraulic generation in the connected reservoir.
- Maximum gross power for closed-cycle pumped storage units is extracted from the information reported by REE (REE, 2014).
- Minimum gross power for closed-cycle pumped storage units is set to zero.
- Maximum power consumed (pumping mode) by hydraulic generators in the connected reservoir and by closed-cycle pumped storage units is estimated as 2.9 GW and 2.7 GW, respectively, according to data from REE (REE, 2009).
- Minimum power consumed (pumping mode) is set to zero for both aggregated reservoirs considered in the model.

Following the guidelines explained above, these input data are collected for each scenario (refer to section 3.2) and presented in Annex A.

c) Reservoir limits  $w_{h,p}^{max}$ ,  $w_{h,p}^{min}$

Maximum and minimum limits for the hydraulic reservoirs are included in the model according to data available in references (REE, 2015b), (Consejería de Economía y Hacienda Comunidad de Madrid, 2011) and (EURELECTRIC, 2011), and they are summarized in Table 1.

| Reservoir level | Connected reservoir | Isolated reservoir |
|-----------------|---------------------|--------------------|
| Maximum [GWh]   | 18538               | 70                 |
| Minimum [GWh]   | 4000                | 0                  |

**Table 1: Maximum and minimum limits for hydraulic reservoirs in the model**

d) Inflows  $i_{h,p}$

Inflows are introduced in the model to represent the hydraulicity during a specific period, this is, the amount of available hydroelectric production once that water supplies for irrigation or other uses than electric production are deducted.

In the model, data from average hydroelectric producible per month and hydraulicity reported by REE (REEAvance14) are used to determine the inflows received by the connected reservoir during each period (week). The average producible (monthly values) is scaled by the producible hydroelectric index considered in each scenario and distributed over the periods considered in the model (proportionally to the number of days per month assigned to each period), see Table 2 and Table 3 below and refer to section 3.2.

| Month     | Average producible [GWh/day] |
|-----------|------------------------------|
| January   | 124                          |
| February  | 145                          |
| March     | 108                          |
| April     | 99                           |
| May       | 89                           |
| June      | 71                           |
| July      | 29                           |
| August    | 14                           |
| September | 20                           |
| October   | 46                           |
| November  | 71                           |
| December  | 98                           |

**Table 2: Average producible hydroelectric energy in Spain**

| Year | GWh   | Index | Probability of being exceeded (%) |
|------|-------|-------|-----------------------------------|
| 2010 | 36174 | 1.29  | 16                                |
| 2011 | 22506 | 0.81  | 74                                |
| 2012 | 12722 | 0.46  | 100                               |
| 2013 | 32631 | 1.18  | 25                                |
| 2014 | 32655 | 1.18  | 25                                |

**Table 3: Annual producible hydroelectric energy in Spain**

The inflows received by the isolated reservoir are neglected.

e) Fuel consumption terms for thermal units  $\alpha_t, \beta_t, \gamma_t, \theta_t$

The different terms of fuel consumption for thermal units (incremental term  $\alpha_t$ , fixed term  $\beta_t$ , start-up fuel consumption  $\gamma_t$  and shut-down fuel consumption  $\theta_t$ ) are considered in the model according to reference (Soler, 2012) and presented in Annex B.

These parameters intend to model the amount of fuel consumed by thermal generators: the incremental term (MTh per GWh) represents the quantity required to produce one unit of energy, the fixed term (MTh per hour) expresses the amount required during one hour of operation and the start-up and shut-down terms (MTh) indicate the quantity spent to start and stop the machines.

f) Gross to net power conversion factor  $k_g$

These factors are used to internalise the amount of power consumed by the auxiliary systems of the plant, in order to determine the net power that is actually delivered by generators. The conversion factors for the different technologies used in the model are obtained from references (MINETUR, 2012) and (IDAE, 2014), and they are summarized in Table 4.

| Technology     | Conversion factor |
|----------------|-------------------|
| Nuclear        | 0.96              |
| Coal           | 0.95              |
| Combined cycle | 0.95              |
| Gas            | 0.95              |
| Hydraulic      | 0.98              |
| Others         | 0.96              |

**Table 4: Gross to net power conversion factors per technology**

g) Efficiency of the pumping-turbine cycle  $k_g$

This value is used to model the losses in the pumping-turbine cycle, this is, not all the energy consumed in the pumping stage can be delivered by the hydraulic units. These values are estimated as 0.7 for both reservoirs.

h) Fuel costs for thermal units  $f_t$

Fuel costs (expressed in k€ per MTh) for uranium, coal and gas are obtained from market data and projections available in references (Bureau of Resources and Energy Economics, 2014), (MIBEL, 2015), (European Commission, 2014). The resulting prices for each scenario are summarized in section 3.2.

Some additional considerations are indicated below:

- The relationship between the uranium price and the associated cost in nuclear plant is derived from data reported by World Nuclear Association (WNA, 2015), see Figure 11.

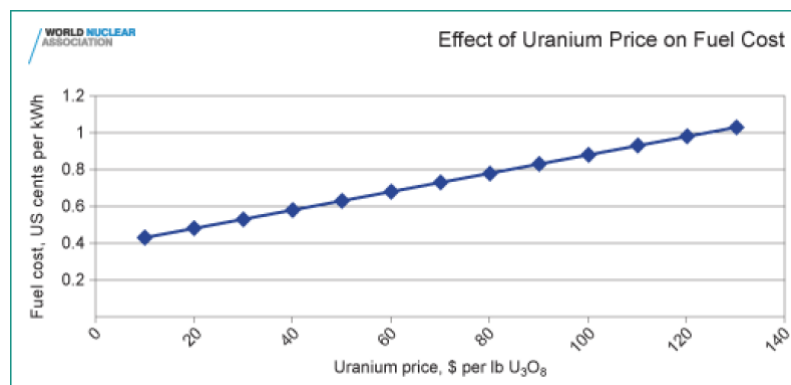


Figure 11: Effect of uranium price on fuel cost for a typical US plant (Source WNA)

- Average fuel prices are obtained from market data in the first quarter of 2015 for API2 and TTF indexes for coal and gas (or from projections from the European Commission (European Commission, 2013) in case of future scenarios).
- Additional logistic cost for coal is considered 10 €/ton according to information available in reference (IEA, 2014).

i) Variable operation and maintenance costs  $o_g$

These values (expressed in k€ per GWh) incorporate other variable costs different from fuel in the objective function. The variable O&M costs for the different technologies used in the model are indicated in Table 5. They are obtained from the following references:

- (UNESA, 2007) for costs for nuclear, coal, combined cycle and integrated gasification combined cycle (IGCC) units.
- (CNE, 2010) for costs for hydraulic, small hydro, wind, solar photovoltaic, solar thermoelectric, non-renewable thermal and renewable thermal units.

| Technology            | O&M cost [k€/GWh] |
|-----------------------|-------------------|
| Nuclear               | 10.2              |
| Coal                  | 4.9               |
| Combined cycle        | 4.5               |
| IGCC                  | 12.9              |
| Hydraulic             | 12.29             |
| Wind                  | 17.4              |
| Solar photovoltaic    | 44.9              |
| Solar thermoelectric  | 114.2             |
| Small hydro           | 17.1              |
| Non-renewable thermal | 63.2              |
| Renewable thermal     | 36                |

**Table 5: Variable operation and maintenance costs per technology**

j) Emission allowance price  $pc_{CO_2}$

CO<sub>2</sub> price (expressed in k€ per ton) is obtained from market data available in EEX (EEX, 2015), and from projections published by the European Commission (European Commission, 2013), see section 3.2.

k) CO<sub>2</sub> emissions per technology  $emis_g$

CO<sub>2</sub> emissions (expressed in ton per GWh) are introduced in the model in order to internalize the environmental costs associated with the production of electricity with each type of technology, since power plants are required to purchase the emission allowances equivalent to the amount of CO<sub>2</sub> generated during production.

The resulting values considered in the model, extracted from data reported by REE (REE, 2015a), are indicated in Table 6.

| Technology            | CO <sub>2</sub> emissions [ton/GWh] |
|-----------------------|-------------------------------------|
| Nuclear               | 0                                   |
| Coal                  | 950                                 |
| Combined cycle        | 370                                 |
| Gas                   | 700                                 |
| Hydraulic             | 0                                   |
| Wind                  | 0                                   |
| Solar photovoltaic    | 0                                   |
| Solar thermoelectric  | 0                                   |
| Small hydro           | 0                                   |
| Non-renewable thermal | 370                                 |
| Renewable thermal     | 0                                   |

**Table 6: CO<sub>2</sub> emissions per technology**

l) Fixed operation and maintenance costs for combined cycles  $f_{oc}$

Fixed operation costs (expressed in k€ per GW) are used to model the potential savings derived from mothballing decisions for combined cycles. These costs are due to the fixed expenses required for the availability of facilities for operation and they are incurred even if they do not produce any power.

Fixed O&M cost for combined cycles is considered an annualized value equal to 31300 k€/GW (13000 k€/GW for the fixed term of operation and maintenance expenses plus 18300 k€/GW corresponding to the gas access tariff) in accordance with data reported by CNMC (CNE, 2012).

Fixed operation costs for other technologies are not taken into account in the model since they do not impact on mothballing decisions.

m) Demand  $d_{n,s,p}$

Input data to determine electricity demand (GW) is obtained from the information system of the Spanish System Operator (REE, 2015b). Data for the year 2014 was collected and processed in order to distribute the hourly values in load blocks that represent the behaviour of demand during each period (week). The process is explained below:

- Hourly demand values for 2014 are assigned to the different weeks (periods) of the year and scaled by a demand growth factor that represent the variation of electricity consumption considered in each scenario, see section 3.2.

- Weeks are divided in working days and non-working days (sub-periods)
- Days are subsequently divided in blocks according to the value of demand (load level). In this thesis they are used five load levels for working days (super-peak, peak, plateau, valley, super-valley) and four load levels for non-working days (peak, plateau, valley, super-valley).
- Demand values are rearranged (ordered) within the two sub-periods of the week according to their load level.
- Average demand values for each period, sub-period and level are computed taking into account the number of hours of each level. The length of load blocks considered in the model is included in Table 7 of the following section.
- The variation of the shape of demand curve over the years is neglected and, therefore, the assignment of periods, subperiods and levels is the same for all the scenarios considered in the model.

According to this, demand values for each scenario (refer to section 3.2) are obtained and included in Annex C.

n) Length of load blocks  $a_{n,s,p}$

The length of load blocks (expressed in hours) for the scenarios considered in the thesis is presented below in Table 7.

| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
|        | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 1      | 8                     | 28     | 32     | 12     | 16     | 24     | 26     | 11     | 11     |
| 2      | 8                     | 28     | 32     | 12     | 16     | 24     | 26     | 11     | 11     |
| 3      | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 4      | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 5      | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 6      | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 7      | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 8      | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 9      | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 10     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |

| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 11     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 12     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 13     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 14     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 15     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 16     | 6                     | 21     | 24     | 9      | 12     | 34     | 32     | 15     | 15     |
| 17     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 18     | 8                     | 28     | 32     | 12     | 16     | 24     | 26     | 11     | 11     |
| 19     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 20     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 21     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 22     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 23     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 24     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 25     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 26     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 27     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 28     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 29     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 30     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 31     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 32     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 33     | 8                     | 28     | 32     | 12     | 16     | 24     | 26     | 11     | 11     |
| 34     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 35     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 36     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 37     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 38     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 39     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 40     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 41     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 42     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |



| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 43     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 44     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 45     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 46     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 47     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 48     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 49     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 50     | 8                     | 28     | 32     | 12     | 16     | 24     | 26     | 11     | 11     |
| 51     | 10                    | 35     | 40     | 15     | 20     | 14     | 20     | 7      | 7      |
| 52     | 8                     | 28     | 32     | 12     | 16     | 24     | 26     | 11     | 11     |

**Table 7: Length of load blocks for each period, sub-period and load block**

o) Thermal gap *thgap*

The thermal gap (expressed in GW) is required in order to constraint the minimum dispatchable generation required by the system. The values used in the model are estimated according to historical values for CCGT, coal and gas production available in (REE, 2015b).

p) Renewable, cogeneration and waste-to-energy generation *res*

The methodology followed to determine the production patterns for renewable, cogeneration and waste-to-energy generation (expressed in GW) is explained below:

- Hourly production values during the year 2014 (obtained from (REE, 2015b)) are assigned to the different weeks (periods) of the year and multiplied by a scale factor that represent the variation of installed power considered for each generation technology and scenario, see section 3.2. This step is applicable for cogeneration, waste-to-energy and all renewable generation except solar photovoltaic.
- In case of solar photovoltaic, hourly production is obtained multiplying the scale power factor considered for each scenario by the hourly duty factors defined in Annex IV of RD 413/2014 (RD 413/2014, 2014). The values considered in the model are the ones that correspond to the climatic zone 4.

- Scaled hourly production values are rearranged according to the load blocks defined in the model, and the average values for each period, sub-period and level are computed taking into account the length of each block.

Production patterns for renewable, cogeneration and waste-to-energy generation for each scenario (refer to section 3.2) are included in Annex D.

### 3.1.3 Objective function

The objective function of the “Midterm planning model” proposed in this thesis (refer to equation (1) in section 3.1.1) computes the operation costs incurred by the units of the system to satisfy demand and technical constraints. The objective is to determine the optimal generation schedule that minimize the aforementioned operation costs.

The operation costs (expressed in k€) comprise fuel costs of the thermal units, variable operation costs for all generators (associated with CO<sub>2</sub> emissions and with operation and maintenance) and fixed operation costs for combined cycles that are available (not mothballed).

### 3.1.4 Constraints

The set of constraints considered in the model (refer to equations (3)-(15) in section 3.1.1) are summarized below:

- Demand balance constraint: expresses the equilibrium between supply (production of thermal, hydraulic and renewable generators) and demand, for each period, sub-period and level of the time horizon considered (one year).
- Power limits constraints: define the feasible range of production for generation units between their operation limits.
- Reservoir management constraints: expresses the energy balance in the reservoirs during each period. The energy stored at the end of the period depends on the energy available in the previous period, the inflows received, the energy produced and the energy returned to the reservoir by pumping.
- Reservoir limits constraints: define the maximum and minimum levels in the reservoir according to their physical capacity.
- Mothballing constraints: define the relationship between mothballing decisions and production. This is, in case of one unit is mothballed, its production is set to zero.

- Thermal gap constraint: expresses the requirements for dispatchable generation. This is, the available generation obtained from dispatchable sources (combined cycles, coal and gas) shall be above the thermal gap considered in the model.
- Relationship between commitment state and start-up/shut-down decisions for thermal generators: defines the dynamics associated with start-up/shut-down decisions within subperiods and in the transition between subperiods. Start-ups and shut-downs are only allowed in the transitions from working days to non-working days.

### 3.1.5 Variables

The following variables are considered in the model:

- Decision variables  $q_{g,n,s,p}, b_{h,n,s,p}$ : positive variables that determine the power (expressed in GW) produced and pumped by the generators in each period, sub-period and level.
- State variables  $w_{h,p}$ : positive variables that represent the energy (expressed in GWh) stored in the reservoirs at the end of each period.
- Decision variables  $y_{t,s,p}, z_{t,s,p}$ : binary variables that decide the commitment of thermal units representing their start-ups and shut-downs, respectively.
- State variables  $u_{t,s,p}$ : binary variables that represent the commitment state of thermal units. They are linked with the start-up and shut-down decisions stated above.
- Decision variables  $m_{gccgt}$ : binary variables that determine mothballing decisions for combined cycles. Its value is 0 for the facilities that are mothballed and 1 for the ones that are available for production (not mothballed).

### 3.1.6 Model assumptions

The assumptions used in the model are indicated below:

- Centralised environment, where decisions are taken by a central agent (i.e. system operator) who is responsible for the exploitation of generation resources and whose decisions are aimed to minimize the operational costs incurred by the system.
- Single node approach, where transmission network is not modelled and grid constraints are not considered.

- Events are modelled through load blocks instead of chronologically, with start-ups and shut-downs of units limited to the transitions between working days and non-working days.
- The shape of demand curve is considered constant over the time horizon, this is, the distribution of load levels and sub-periods within each period of the horizon is assumed to be the same in different scenarios and, therefore, a unique distribution of periods, sub-periods and load levels is used.
- Two aggregated reservoirs (instead of detail representation of water basins) to model the behaviour of all hydro units.
- Fuel consumption for thermal units is assumed to be linear.
- Deterministic approach: uncertainty related to input data is neglected. Instead, they are used forecasts or estimations for input data such as technical characteristics of generation units, demand, fuel and emission allowance costs, hydrology and production for renewable, cogeneration and waste-to-energy units.
- Evolution of input data over the time horizon is also estimated, when applicable.
- Availability of units in terms of scheduled maintenance or unexpected outage is not taken into account.
- International electricity exchanges or with extra-peninsular systems are not included in the model.
- Fixed operation costs incurred by other technologies different than combined cycles are not taken into account, since they would not impact on the mothballing decisions or scheduling.

### **3.2 Development of alternative scenarios**

In this section the different scenarios considered in the model are defined. The main guidelines are explained below:

- Two yearly time horizon are considered corresponding to the years 2015 and 2020, respectively.
- Three scenarios are generated for the aim of this thesis. In the base case scenario the midterm generation planning model is used to determine the optimal scheduling in 2015,

assuming that combined cycles are not allowed to mothball capacity. The other two scenarios consider the problem of generation planning for the years 2015 and 2020, taking into account that mothballing decisions are allowed.

| Scenario                        |
|---------------------------------|
| 2015 without mothballing        |
| 2015 with mothballing decisions |
| 2020 with mothballing decisions |

**Table 8: Base case and alternative scenarios**

- Generation mixes for each scenario are indicated in Table 9 and Table 10. They are based on data from (REE, 2014) and projections from (Ministerio de Industria, Turismo y Comercio, 2014).

| Technology                          | Installed power [GW] |
|-------------------------------------|----------------------|
| Nuclear                             | 7.865                |
| Coal                                | 10.635               |
| Combined cycle                      | 25.357               |
| IGCC                                | 0.32                 |
| Hydraulic (including mixed pumping) | 15.039               |
| Closed-cycle pumping                | 2.747                |
| Wind                                | 22.845               |
| Solar photovoltaic                  | 4.428                |
| Solar thermoelectric                | 2.3                  |
| Small hydro                         | 2.105                |
| Non-renewable thermal               | 7.075                |
| Renewable thermal                   | 1.01                 |

**Table 9: Generation mix. Scenarios 2015**

| Technology                          | Installed power [GW] |
|-------------------------------------|----------------------|
| Nuclear                             | 7.865                |
| Coal                                | 10.635               |
| Combined cycle                      | 25.357               |
| IGCC                                | 0.32                 |
| Hydraulic (including mixed pumping) | 15.288               |
| Closed-cycle pumping                | 3.77                 |
| Wind                                | 27.65                |
| Solar photovoltaic                  | 5.79                 |
| Solar thermoelectric                | 2.3                  |
| Small hydro                         | 2.3                  |
| Non-renewable thermal               | 7.39                 |
| Renewable thermal                   | 1.254                |

**Table 10: Generation mix. Scenario 2020**

- In all scenarios, the operation of Garoña nuclear power plant is not considered (even though the facility is included within the generation mixes).
- Additionally, power reductions in coal power plants foreseen in reference (Ministerio de Industria, Turismo y Comercio , 2014) for year 2020 are not taken into account since they are considered of low relevance.
- Annual demand values for each scenario are based on projections from the Spanish System Operator available at (CNMC, 2015) and they are indicated in Table 11 together with their corresponding growth factor.

| Year | Demand [GWh] | Demand growth factor |
|------|--------------|----------------------|
| 2014 | 242282       | -                    |
| 2015 | 251600       | 1.0385               |
| 2020 | 277700       | 1.1462               |

**Table 11: Annual demand. Year 2014 and scenarios 2015 and 2020**

- All scenarios consider low hydraulicity (in accordance with proposed regulation for mothballing mechanisms in Spain) in order to take into account the restrictive conditions that are faced during dry years.

Therefore, according to the methodology explained in section 3.1.2, the average producible values are scaled by the producible hydroelectric index of a year with low hydraulicity and distributed over the periods considered in each scenario, see Table 12 and Table 13.

| Month     | Producible [GWh/day] |
|-----------|----------------------|
| January   | 1768.2               |
| February  | 1867.6               |
| March     | 1540.1               |
| April     | 1366.2               |
| May       | 1269.1               |
| June      | 979.8                |
| July      | 413.5                |
| August    | 199.6                |
| September | 276                  |
| October   | 657                  |
| November  | 979.8                |
| December  | 1397.5               |

**Table 12: Monthly producible hydroelectric energy (index 0.46). Scenarios 2015 and 2020**

| Week | Inflows [GWh] | Week | Inflows [GWh] |
|------|---------------|------|---------------|
| 1    | 375           | 2    | 399           |
| 3    | 399           | 4    | 399           |
| 5    | 419           | 6    | 467           |
| 7    | 467           | 8    | 467           |
| 9    | 433           | 10   | 348           |
| 11   | 348           | 12   | 348           |
| 13   | 348           | 14   | 323           |
| 15   | 319           | 16   | 319           |
| 17   | 319           | 18   | 300           |
| 19   | 287           | 20   | 287           |
| 21   | 287           | 22   | 278           |
| 23   | 229           | 24   | 229           |
| 25   | 229           | 26   | 229           |
| 27   | 113           | 28   | 93            |

| Week | Inflows [GWh] | Week | Inflows [GWh] |
|------|---------------|------|---------------|
| 29   | 93            | 30   | 93            |
| 31   | 73            | 32   | 45            |
| 33   | 45            | 34   | 45            |
| 35   | 45            | 36   | 64            |
| 37   | 64            | 38   | 64            |
| 39   | 64            | 40   | 124           |
| 41   | 148           | 42   | 148           |
| 43   | 148           | 44   | 171           |
| 45   | 229           | 46   | 229           |
| 47   | 229           | 48   | 229           |
| 49   | 316           | 50   | 316           |
| 51   | 316           | 52   | 316           |

**Table 13: Inflows received per period. Scenarios 2015 and 2020**

- Fuel costs for uranium, coal and gas in each scenario are indicated in Table 14, Table 15 and Table 16 below. For the purpose of units' conversion, a euro/dollar exchange rate of 1.12 has been considered.

| Year | Fuel price [\$ / lb U <sub>3</sub> O <sub>8</sub> ] | Fuel cost [US cent / kWh] | Fuel cost [k€ / MTh] |
|------|---|---------------------------|----------------------|
| 2015 | 32  | 0.53                      | 5.50                 |
| 2020 | 60  | 0.67                      | 6.96                 |

**Table 14: Uranium cost. Scenarios 2015 and 2020**

| Year | Fuel price                 | Logistic cost | Fuel cost      |
|------|----------------------------|---------------|----------------|
| 2015 | 54.03 €/ton                | 10 €/ton      | 9.15 k€ / MTh  |
| 2020 | 110.15 €/ton<br>(23 €/boe) | 10 €/ton      | 17.16 k€ / MTh |

**Table 15: Coal cost. Scenarios 2015 and 2020**

| Year | Fuel price                | Fuel cost      |
|------|---------------------------|----------------|
| 2015 | 21.58 €/MWh               | 25.09 k€ / MTh |
| 2020 | 36.47 €/MWh<br>(62 €/boe) | 42.41 k€ / MTh |

**Table 16: Gas cost. Scenarios 2015 and 2020**



- CO<sub>2</sub> emission allowance prices are based on projections from the European Commission (European Commission, 2013), see Figure 12. Prices for the considered scenarios are summarized in Table 17.

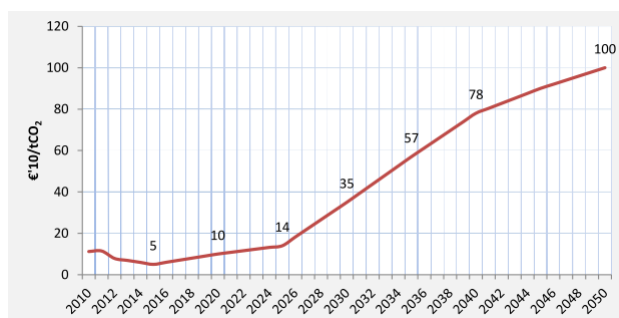


Figure 12: Projections for ETS price (Source European Commission)

| Year | CO <sub>2</sub> price |
|------|-----------------------|
| 2015 | 5 €/tCO <sub>2</sub>  |
| 2020 | 10 €/tCO <sub>2</sub> |

Table 17: CO<sub>2</sub> emission allowance price. Scenarios 2015 and 2020

- Finally, minimum dispatchable generation (thermal gap) is considered in order to analyze the behavior of the system depending on the requirements imposed to dispatchable production, see Table 18.

| Year | Thermal gap [GW] |
|------|------------------|
| 2015 | 23000            |
| 2020 | 23000            |

Table 18: Thermal gap. Scenarios 2015 and 2020

The thermal gap is used to assess the impact of integration of renewable energy sources on mothballing decisions, since dispatchable production requirements depend on the relationship between renewable generation and demand (available dispatchable generation is required by the system in order to substitute renewable generation in case that this is not available).

## 4 Results

In this chapter they are presented the results obtained for the application of the model to the three scenarios considered in the thesis. Specifically, the results are focused on the generation schedule, the contribution of each technology to the energy mix, the operation costs, the amount of CO<sub>2</sub> emissions, the quantity of mothballed power and the level of security of supply.

For the aim of this thesis, the relationship between the installed dispatchable power (not mothballed) and the thermal gap has been selected as an indicator of the level of security of supply.

### 4.1 Model results for the base case

#### 4.1.1 Generation schedule

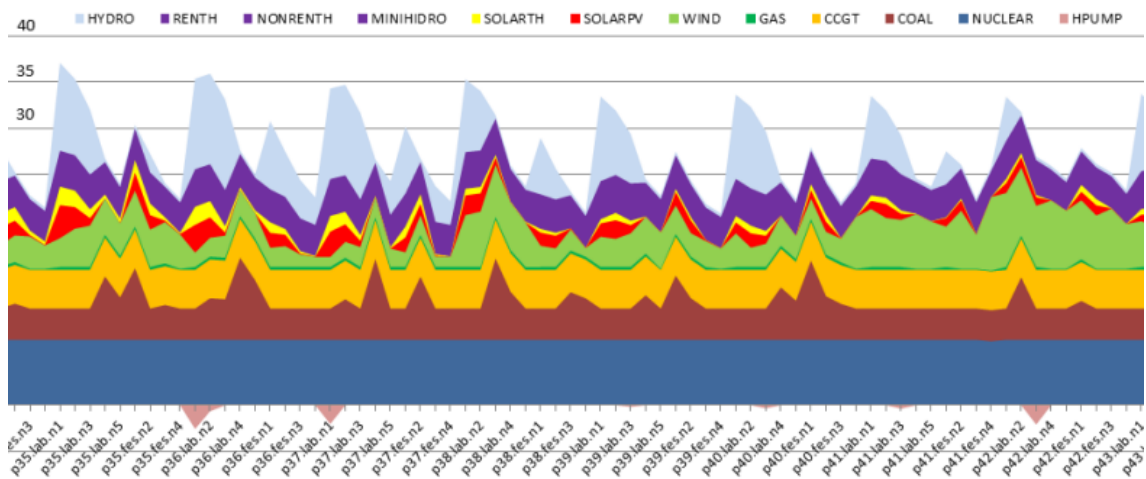


Figure 13: Generation schedule for scenario 2015 without mothballing

## 4.1.2 Energy mix

| Technology            | Production [GWh] |
|-----------------------|------------------|
| Nuclear               | 61942            |
| Coal                  | 35507            |
| Combined cycle        | 36680            |
| IGCC                  | 2140             |
| Wind                  | 50067            |
| Solar photovoltaic    | 8110             |
| Solar thermoelectric  | 5199             |
| Small hydro           | 6782             |
| Non-renewable thermal | 22152            |
| Renewable thermal     | 4699             |
| Hydraulic             | 21016            |
| Pumping               | -2562            |
| <b>TOTAL</b>          | <b>251732</b>    |

Table 19: Energy mix for scenario 2015 without mothballing

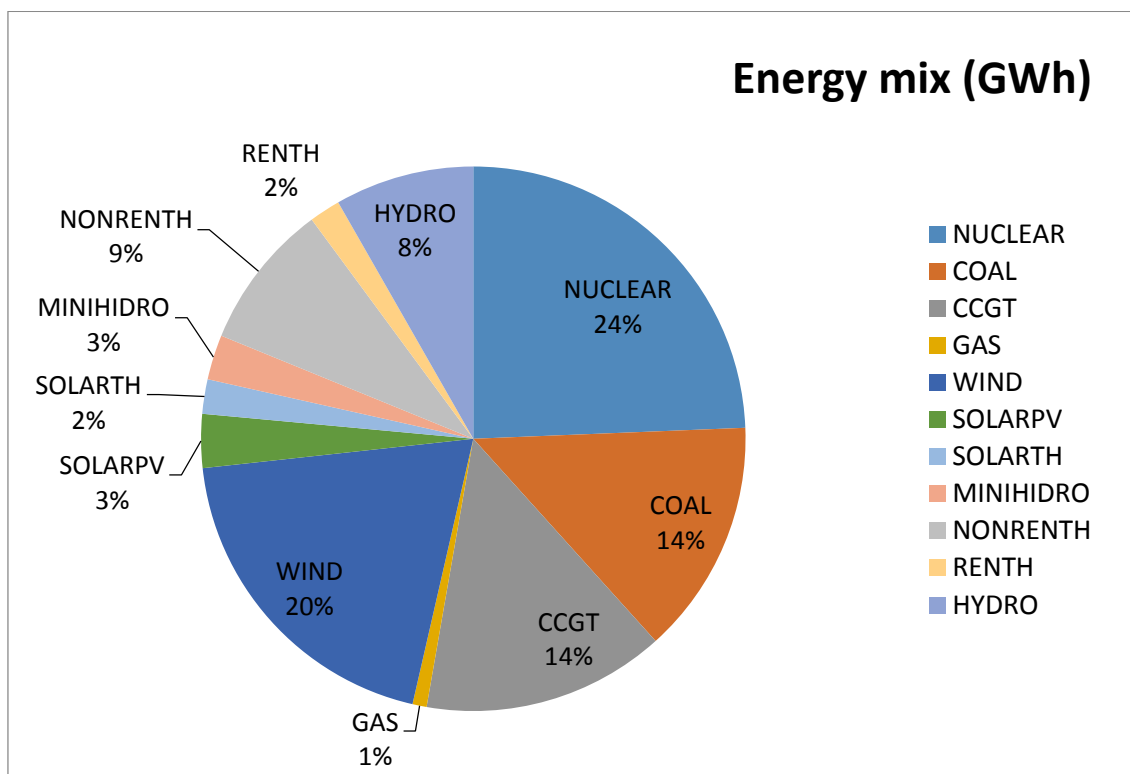


Figure 14: Energy mix for scenario 2015 without mothballing

### 4.1.3 Operation costs

---

**Operation costs**

**9434.6 M€**

---

Table 20: Operation costs for scenario 2015 without mothballing

### 4.1.4 CO<sub>2</sub> emissions

| Technology            | CO <sub>2</sub> emissions [ton] |
|-----------------------|---------------------------------|
| Coal                  | 33731417                        |
| Combined cycle        | 13571488                        |
| IGCC                  | 1497707                         |
| Non-renewable thermal | 8196119                         |
| <b>TOTAL</b>          | <b>56996731</b>                 |

Table 21: CO<sub>2</sub> emissions for scenario 2015 without mothballing

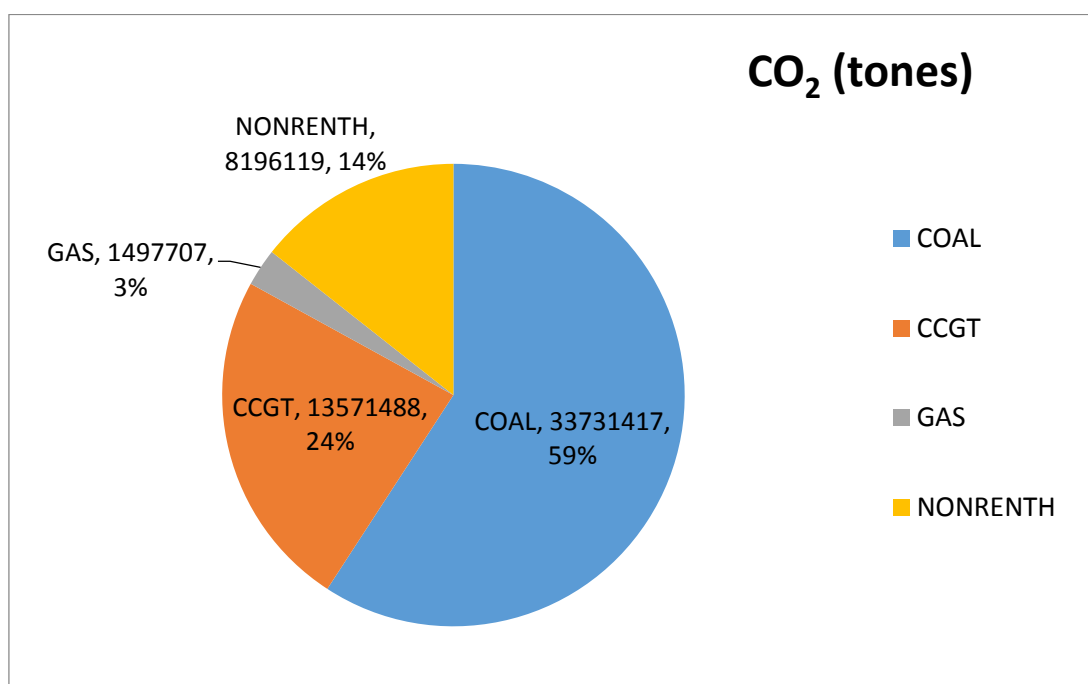


Figure 15: CO<sub>2</sub> emissions for scenario 2015 without mothballing

### 4.1.5 Mothballed power

---

**Mothballed power**

**0 GW**

---

Table 22: Mothballed power for scenario 2015 without mothballing

### 4.1.6 Security of supply

|                         |           |
|-------------------------|-----------|
| Thermal gap             | 23 GW     |
| Available thermal power | 36.312 GW |
| RATIO                   | 1.579     |

Table 23: Available thermal power vs thermal gap for scenario 2015 without mothballing

## 4.2 Scenario analysis

### 4.2.1 Generation schedule

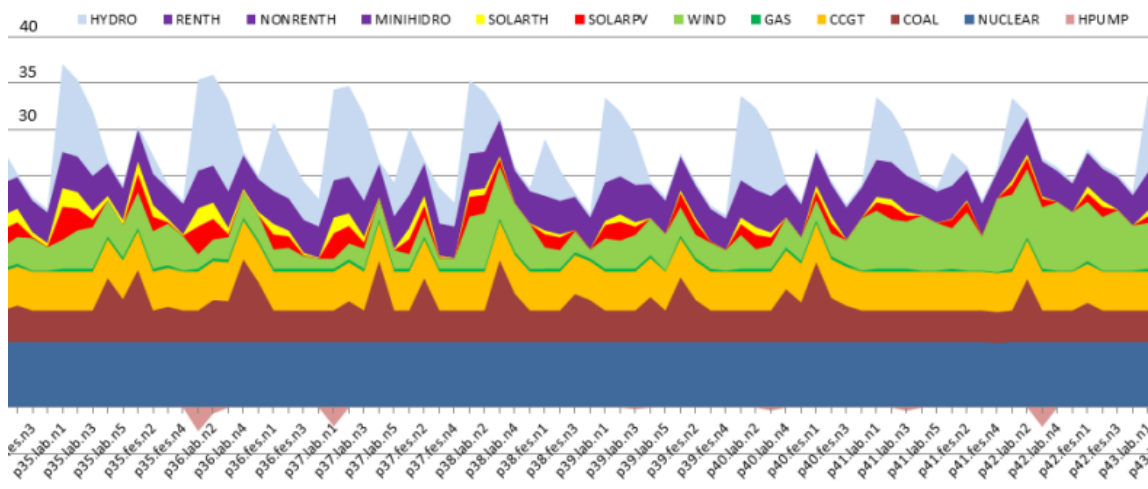


Figure 16: Generation schedule for scenario 2015 with mothballing

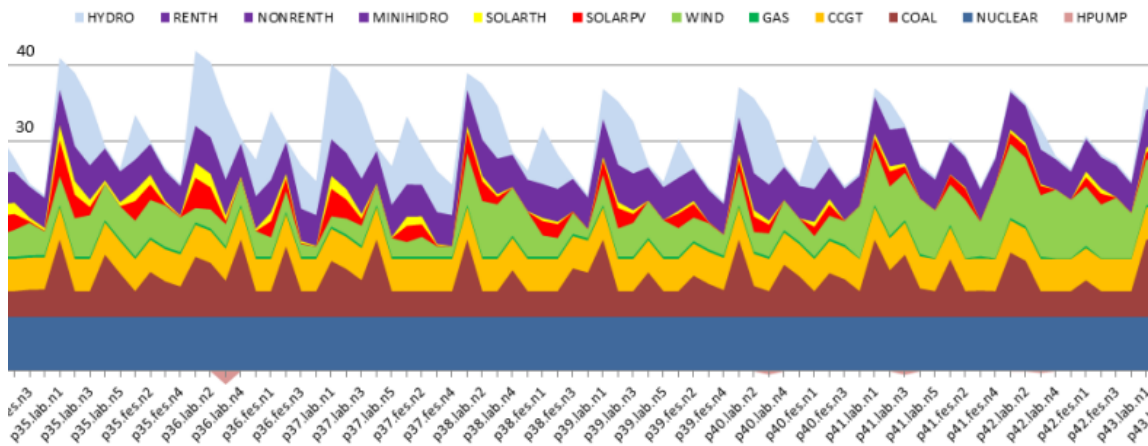


Figure 17: Generation schedule for scenario 2020 with mothballing

## 4.2.2 Energy mix

| Technology            | Production [GWh] |
|-----------------------|------------------|
| Nuclear               | 61942            |
| Coal                  | 35507            |
| Combined cycle        | 36680            |
| IGCC                  | 2140             |
| Wind                  | 50067            |
| Solar photovoltaic    | 8110             |
| Solar thermoelectric  | 5199             |
| Small hydro           | 6782             |
| Non-renewable thermal | 22152            |
| Renewable thermal     | 4699             |
| Hydraulic             | 21016            |
| Pumping               | -2562            |
| <b>TOTAL</b>          | <b>251732</b>    |

Table 24: Energy mix for scenario 2015 with mothballing

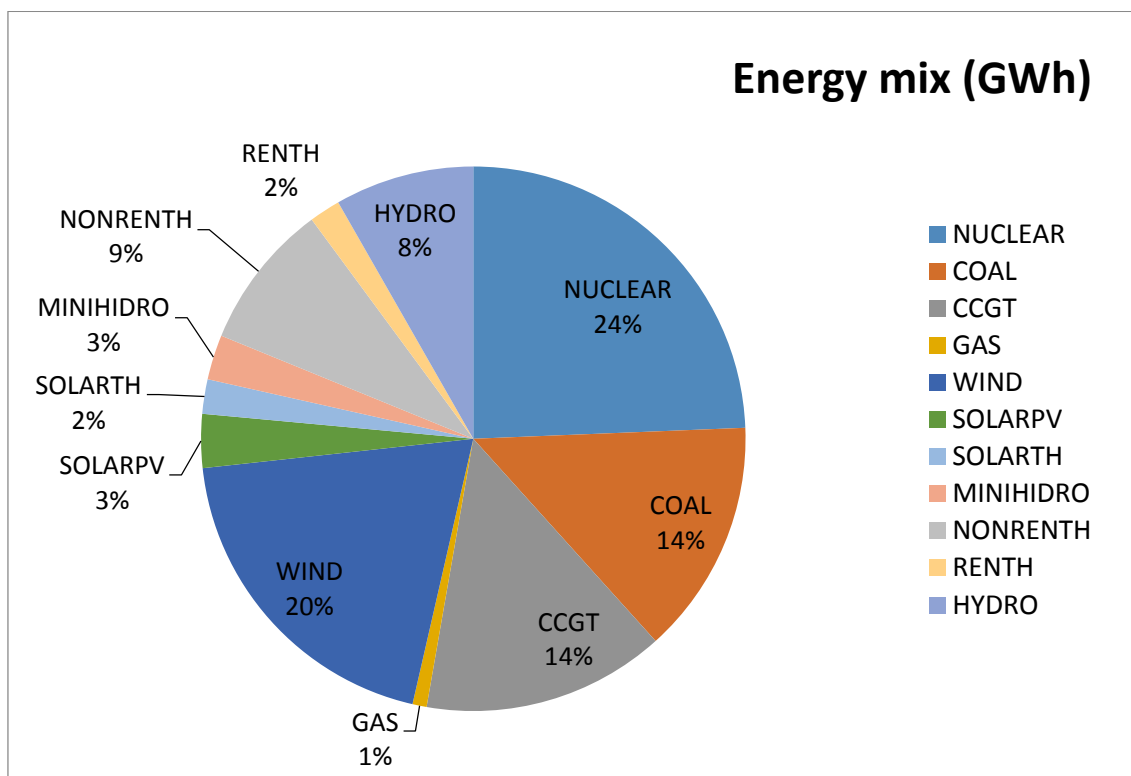


Figure 18: Energy mix for scenario 2015 with mothballing

| Technology            | Production [GWh] |
|-----------------------|------------------|
| Nuclear               | 62000            |
| Coal                  | 42072            |
| Combined cycle        | 36688            |
| IGCC                  | 2220             |
| Wind                  | 60598            |
| Solar photovoltaic    | 10604            |
| Solar thermoelectric  | 5199             |
| Small hydro           | 7411             |
| Non-renewable thermal | 27503            |
| Renewable thermal     | 4908             |
| Hydraulic             | 21041            |
| Pumping               | -2174            |
| <b>TOTAL</b>          | <b>278070</b>    |

Table 25: Energy mix for scenario 2020 with mothballing

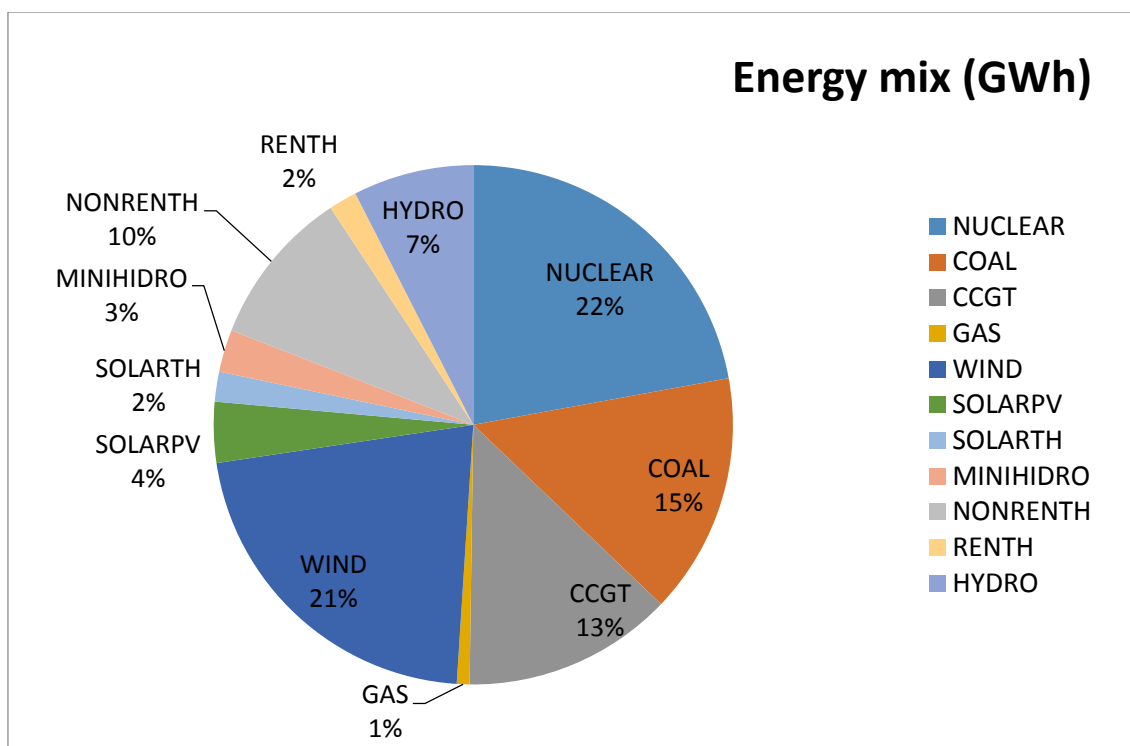


Figure 19: Energy mix for scenario 2020 with mothballing

### 4.2.3 Operation costs

---

**Operation costs**

**9056 M€**

---

**Table 26: Operation costs for scenario 2015 with mothballing**

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**Operation costs**

**12608 M€**

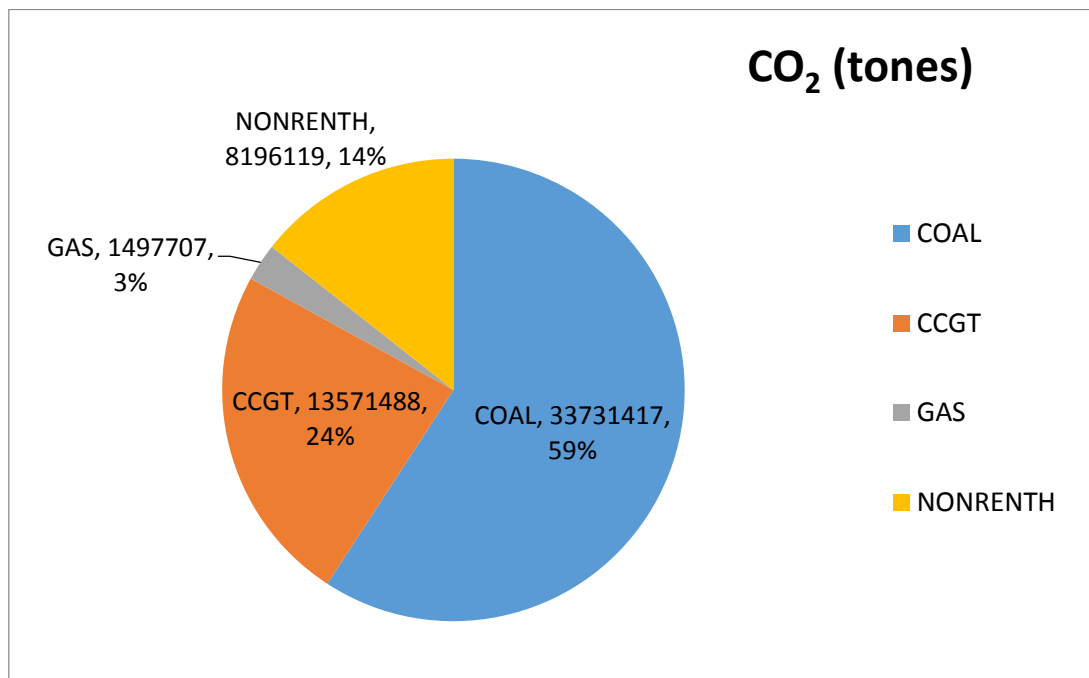
---

**Table 27: Operation costs for scenario 2020 with mothballing**

### 4.2.4 CO<sub>2</sub> emissions

| Technology            | CO <sub>2</sub> emissions [ton] |
|-----------------------|---------------------------------|
| Coal                  | 33731417                        |
| Combined cycle        | 13571488                        |
| IGCC                  | 1497707                         |
| Non-renewable thermal | 8196119                         |
| <b>TOTAL</b>          | <b>56996731</b>                 |

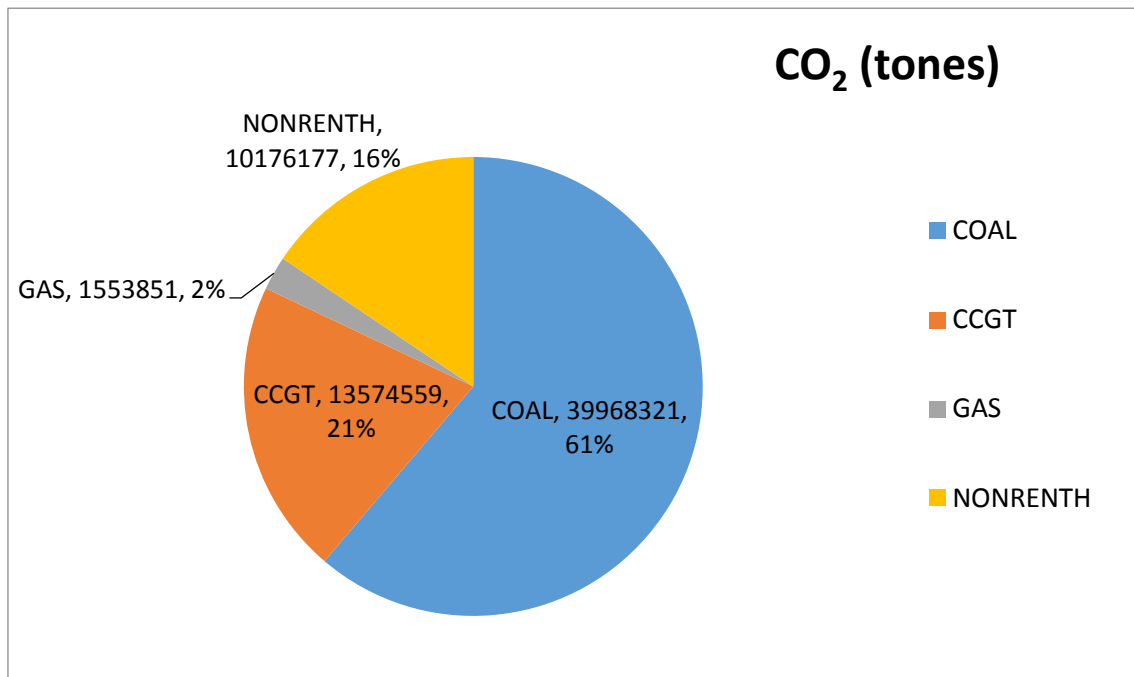
**Table 28: CO<sub>2</sub> emissions for scenario 2015 with mothballing**



**Figure 20: CO<sub>2</sub> emissions for scenario 2015 with mothballing**



| Technology            | CO <sub>2</sub> emissions [ton] |
|-----------------------|---------------------------------|
| Coal                  | 39968321                        |
| Combined cycle        | 13574559                        |
| IGCC                  | 1553851                         |
| Non-renewable thermal | 10176177                        |
| <b>TOTAL</b>          | <b>65272908</b>                 |

Table 29: CO<sub>2</sub> emissions for scenario 2020 with mothballingFigure 21: CO<sub>2</sub> emissions for scenario 2020 with mothballing

#### 4.2.5 Mothballed power

---

**Mothballed power**

**11.7 GW**

---

Table 30: Mothballed power for scenario 2015 with mothballing

---

**Mothballed power**

**12.1 GW**

---

Table 31: Mothballed power for scenario 2020 with mothballing

#### 4.2.6 Security of supply

---

|                                |                |
|--------------------------------|----------------|
| <b>Thermal gap</b>             | <b>23 GW</b>   |
| <b>Available thermal power</b> | <b>24.6 GW</b> |
| <b>RATIO</b>                   | <b>1.070</b>   |

---

**Table 32: Available thermal power vs thermal gap for scenario 2015 with mothballing**

---

|                                |                |
|--------------------------------|----------------|
| <b>Thermal gap</b>             | <b>23 GW</b>   |
| <b>Available thermal power</b> | <b>23.9 GW</b> |
| <b>RATIO</b>                   | <b>1.039</b>   |

---

**Table 33: Available thermal power vs thermal gap for scenario 2020 with mothballing**

## 5 Conclusions

In this chapter they are provided the main findings resulted from the work developed herein, as well as some suggestions for further research.

### 5.1 Discussion of results

The model proposed in this thesis is able to incorporate the dynamics of mothballing decisions for combined cycles in the midterm generation planning. The process followed intends to model on the one hand, the potential savings in operating costs when facilities are allowed to mothball and, on the other hand, the system requirements on dispatchable generation (not all the facilities are allowed to mothball since they serve as a back-up for other generation sources).

The results obtained with the application of the proposed model to the Spanish Systems (refer to section 4) suggest the following findings:

- The two scenarios considered for the year 2015 (with and without mothballing) obtain the same dispatch results and the mothballing decisions do not impact on scheduling or CO<sub>2</sub> emissions.
- Mothballing decisions in the year 2015 do not result in any technological replacement. This indicates that the mothballed power did not have any contribution in the energy mix (due to the excess of installed capacity present in the system).
- Mothballed power for the scenario 2015 accounts for 11.7 GW (considering a thermal gap of 23 GW).
- Mothballing decisions in the scenario considered for the year 2015 are able to reduce the operating costs in 379 M€, due to the savings in fixed operating costs associated with the plants that are mothballed.
- The two scenarios analysed for the year 2015 indicate that the ratio between dispatchable power and thermal gap is reduced from 1.579 to 1.070 in case of mothballing, indicating that dispatchable generation in the first scenario is more than 50% above system requirements (considering the assumptions followed in the model).
- The scenario 2020 is characterised by the increase in demand and in fuel and emission allowance prices, where higher operating costs and CO<sub>2</sub> emissions are obtained.

- The demand increase considered in the scenario 2020 is covered by the increase in renewable production (estimated in the model proportionally to the projected installed power) and by the cheapest thermal available generation (coal in this case). On the other hand, the contribution of nuclear and hydro is reduced within the total mix.
- Mothballed power for the scenario 2020 accounts for 12.1 GW, with associated ratio between dispatchable power and thermal gap of 1.039. This indicates that, taking into account the assumptions followed within this thesis, the increase of demand projected for 2020 is not enough to reinstate mothballed plants between 2015 and 2020. This result could be affected in case that thermal gap would be increased in the considered horizon.

## 5.2 Suggestions for further research

Finally, some suggestions for future developments are indicated below:

- Analysis of relevant network constraints for its incorporation in the proposed model (to exclude the mothballing of generators that are required to solve the system constraints).
- Further developments in the estimation of thermal gap, for example, analysis of its evolution with renewable integration, consideration of demand side management (interruptibility service), etc.
- Incorporation of availability of units in the model, as well as alternative approaches to consider security of supply (with the coverage index for example).
- Analysis of the impact of constraints related to domestic coal consumption for its incorporation in the model.
- Adjustment of the model to consider longer periods of mothballing (more than one year).
- Analysis of the impact of considering hydroelectric and pumping stations as dispatchable generation.
- Extension of the model to foresee also seasonal mothballing and possible application to other power systems.
- Sensitivity analysis to variations in demand, fuel and CO<sub>2</sub> prices and hydraulicity.
- Consideration of the problem of mothballing from the perspective of a market agent and its potential effect on competition.

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**ANNEX A**  
**GENERATION UNITS**

## ANNEX A GENERATION UNITS

| GENERATION UNITS |                          |                          |                          |                          |
|------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| UNIT             | YEAR 2015                |                          | YEAR 2020                |                          |
|                  | Maximum gross power [GW] | Minimum gross power [GW] | Maximum gross power [GW] | Minimum gross power [GW] |
| NUC_ALM1         | 1.049                    | 0.350                    | 1.049                    | 0.350                    |
| NUC_ALM2         | 1.044                    | 0.348                    | 1.044                    | 0.348                    |
| NUC_ASC1         | 1.033                    | 0.344                    | 1.033                    | 0.344                    |
| NUC_ASC2         | 1.027                    | 0.342                    | 1.027                    | 0.342                    |
| NUC_COF          | 1.092                    | 0.364                    | 1.092                    | 0.364                    |
| NUC_GAR          | 0.466                    | 0.155                    | 0.466                    | 0.155                    |
| NUC_TRI          | 1.067                    | 0.356                    | 1.067                    | 0.356                    |
| NUC_VAN2         | 1.087                    | 0.362                    | 1.087                    | 0.362                    |
| COAL_ABO1        | 0.36                     | 0.120                    | 0.36                     | 0.120                    |
| COAL_ABO2        | 0.556                    | 0.185                    | 0.556                    | 0.185                    |
| COAL_ANL         | 0.365                    | 0.122                    | 0.365                    | 0.122                    |
| COAL_COM2        | 0.148                    | 0.049                    | 0.148                    | 0.049                    |
| COAL_COM3        | 0.337                    | 0.112                    | 0.337                    | 0.112                    |
| COAL_COM4        | 0.359                    | 0.120                    | 0.359                    | 0.120                    |
| COAL_COM5        | 0.356                    | 0.119                    | 0.356                    | 0.119                    |
| COAL_GUA1        | 0.155                    | 0.052                    | 0.155                    | 0.052                    |
| COAL_GUA2        | 0.361                    | 0.120                    | 0.361                    | 0.120                    |
| COAL_LRO1        | 0.284                    | 0.095                    | 0.284                    | 0.095                    |
| COAL_LRO2        | 0.371                    | 0.124                    | 0.371                    | 0.124                    |
| COAL_LAD4        | 0.358                    | 0.119                    | 0.358                    | 0.119                    |
| COAL_LIT1        | 0.577                    | 0.192                    | 0.577                    | 0.192                    |
| COAL_LIT2        | 0.582                    | 0.194                    | 0.582                    | 0.194                    |
| COAL_LBA         | 0.589                    | 0.196                    | 0.589                    | 0.196                    |
| COAL_MEI         | 0.563                    | 0.188                    | 0.563                    | 0.188                    |
| COAL_NAR1        | 0.065                    | 0.022                    | 0.065                    | 0.022                    |
| COAL_NAR2        | 0.166                    | 0.055                    | 0.166                    | 0.055                    |
| COAL_NAR3        | 0.364                    | 0.121                    | 0.364                    | 0.121                    |
| COAL_PNU3        | 0.324                    | 0.108                    | 0.324                    | 0.108                    |
| COAL_PUE1        | 0.369                    | 0.123                    | 0.369                    | 0.123                    |



## GENERATION UNITS

| UNIT      | YEAR 2015                |                          | YEAR 2020                |                          |
|-----------|--------------------------|--------------------------|--------------------------|--------------------------|
|           | Maximum gross power [GW] | Minimum gross power [GW] | Maximum gross power [GW] | Minimum gross power [GW] |
| COAL_PUE2 | 0.366                    | 0.122                    | 0.366                    | 0.122                    |
| COAL_PUE3 | 0.366                    | 0.122                    | 0.366                    | 0.122                    |
| COAL_PUE4 | 0.367                    | 0.122                    | 0.367                    | 0.122                    |
| COAL_PLL  | 0.221                    | 0.074                    | 0.221                    | 0.074                    |
| COAL_SOT2 | 0.254                    | 0.085                    | 0.254                    | 0.085                    |
| COAL_SOT3 | 0.35                     | 0.117                    | 0.35                     | 0.117                    |
| COAL_TER1 | 0.368                    | 0.123                    | 0.368                    | 0.123                    |
| COAL_TER2 | 0.368                    | 0.123                    | 0.368                    | 0.123                    |
| COAL_TER3 | 0.366                    | 0.122                    | 0.366                    | 0.122                    |
| CCGT_ACE3 | 0.392                    | 0.131                    | 0.392                    | 0.131                    |
| CCGT_ACE4 | 0.379                    | 0.126                    | 0.379                    | 0.126                    |
| CCGT_ALG3 | 0.831                    | 0.277                    | 0.831                    | 0.277                    |
| CCGT_AMO  | 0.795                    | 0.265                    | 0.795                    | 0.265                    |
| CCGT_ARC1 | 0.396                    | 0.132                    | 0.396                    | 0.132                    |
| CCGT_ARC2 | 0.379                    | 0.126                    | 0.379                    | 0.126                    |
| CCGT_ARC3 | 0.844                    | 0.281                    | 0.844                    | 0.281                    |
| CCGT_ARR1 | 0.402                    | 0.134                    | 0.402                    | 0.134                    |
| CCGT_ARR2 | 0.397                    | 0.132                    | 0.397                    | 0.132                    |
| CCGT_BIZ  | 0.8                      | 0.267                    | 0.8                      | 0.267                    |
| CCGT_BES3 | 0.419                    | 0.140                    | 0.419                    | 0.140                    |
| CCGT_BES4 | 0.407                    | 0.136                    | 0.407                    | 0.136                    |
| CCGT_BES5 | 0.873                    | 0.291                    | 0.873                    | 0.291                    |
| CCGT_GIB1 | 0.393                    | 0.131                    | 0.393                    | 0.131                    |
| CCGT_GIB2 | 0.388                    | 0.129                    | 0.388                    | 0.129                    |
| CCGT_CAR1 | 0.425                    | 0.142                    | 0.425                    | 0.142                    |
| CCGT_CAR2 | 0.425                    | 0.142                    | 0.425                    | 0.142                    |
| CCGT_CAR3 | 0.419                    | 0.140                    | 0.419                    | 0.140                    |
| CCGT_CJN1 | 0.429                    | 0.143                    | 0.429                    | 0.143                    |
| CCGT_CJN2 | 0.381                    | 0.127                    | 0.381                    | 0.127                    |
| CCGT_CJN3 | 0.426                    | 0.142                    | 0.426                    | 0.142                    |
| CCGT_CLN3 | 0.793                    | 0.264                    | 0.793                    | 0.264                    |

## GENERATION UNITS

| UNIT      | YEAR 2015                |                          | YEAR 2020                |                          |
|-----------|--------------------------|--------------------------|--------------------------|--------------------------|
|           | Maximum gross power [GW] | Minimum gross power [GW] | Maximum gross power [GW] | Minimum gross power [GW] |
| CCGT_CLN4 | 0.854                    | 0.285                    | 0.854                    | 0.285                    |
| CCGT_CNO  | 0.798                    | 0.266                    | 0.798                    | 0.266                    |
| CCGT_COL4 | 0.398                    | 0.133                    | 0.398                    | 0.133                    |
| CCGT_EFG1 | 0.409                    | 0.136                    | 0.409                    | 0.136                    |
| CCGT_EFG2 | 0.408                    | 0.136                    | 0.408                    | 0.136                    |
| CCGT_EFG3 | 0.402                    | 0.134                    | 0.402                    | 0.134                    |
| CCGT_ESC3 | 0.818                    | 0.273                    | 0.818                    | 0.273                    |
| CCGT_ESCP | 0.283                    | 0.094                    | 0.283                    | 0.094                    |
| CCGT_ESC6 | 0.831                    | 0.277                    | 0.831                    | 0.277                    |
| CCGT_MAL1 | 0.421                    | 0.140                    | 0.421                    | 0.140                    |
| CCGT_PAL1 | 0.394                    | 0.131                    | 0.394                    | 0.131                    |
| CCGT_PAL2 | 0.396                    | 0.132                    | 0.396                    | 0.132                    |
| CCGT_PAL3 | 0.398                    | 0.133                    | 0.398                    | 0.133                    |
| CCGT_PLV1 | 0.426                    | 0.142                    | 0.426                    | 0.142                    |
| CCGT_PLV2 | 0.421                    | 0.140                    | 0.421                    | 0.140                    |
| CCGT_PUE  | 0.87                     | 0.290                    | 0.87                     | 0.290                    |
| CCGT_PUB1 | 0.447                    | 0.149                    | 0.447                    | 0.149                    |
| CCGT_PUB2 | 0.445                    | 0.148                    | 0.445                    | 0.148                    |
| CCGT_SAB3 | 0.397                    | 0.132                    | 0.397                    | 0.132                    |
| CCGT_SAG1 | 0.417                    | 0.139                    | 0.417                    | 0.139                    |
| CCGT_SAG2 | 0.42                     | 0.140                    | 0.42                     | 0.140                    |
| CCGT_SAG3 | 0.419                    | 0.140                    | 0.419                    | 0.140                    |
| CCGT_SRO1 | 0.397                    | 0.132                    | 0.397                    | 0.132                    |
| CCGT_SRO2 | 0.402                    | 0.134                    | 0.402                    | 0.134                    |
| CCGT_STU4 | 0.403                    | 0.134                    | 0.403                    | 0.134                    |
| CCGT_RIB4 | 0.432                    | 0.144                    | 0.432                    | 0.144                    |
| CCGT_RIB5 | 0.434                    | 0.145                    | 0.434                    | 0.145                    |
| CCGT_TARE | 0.4                      | 0.133                    | 0.4                      | 0.133                    |
| CCGT_TARP | 0.424                    | 0.141                    | 0.424                    | 0.141                    |
| GAS_ECG   | 0.32                     | 0.107                    | 0.32                     | 0.107                    |
| WIND      | 22.845                   | 0.000                    | 27.65                    | 0.000                    |

## GENERATION UNITS

| UNIT      | YEAR 2015                |                          | YEAR 2020                |                          |
|-----------|--------------------------|--------------------------|--------------------------|--------------------------|
|           | Maximum gross power [GW] | Minimum gross power [GW] | Maximum gross power [GW] | Minimum gross power [GW] |
| SOLARPV   | 4.428                    | 0.000                    | 5.79                     | 0.000                    |
| SOLARTH   | 2.3                      | 0.000                    | 2.3                      | 0.000                    |
| MINIHYDRO | 2.105                    | 0.000                    | 2.3                      | 0.000                    |
| NONRENTH  | 7.075                    | 0.000                    | 7.39                     | 0.000                    |
| RENTH     | 1.01                     | 0.000                    | 1.254                    | 0.000                    |
| HYD_RES   | 10                       | 0.400                    | 10                       | 0.400                    |
| HYD_PUM   | 2.747                    | 0.000                    | 3.77                     | 0.000                    |

**ANNEX B**  
**PARAMETERS OF THERMAL UNITS**

## ANNEX B PARAMETERS OF THERMAL UNITS

| PARAMETERS OF THERMAL UNITS $\alpha_t, \beta_t, \gamma_t, \theta_t$ |                      |                     |                      |                      |
|---|----------------------|---------------------|----------------------|----------------------|
| UNIT  | $\alpha_t$ [MTh/GWh] | $\beta_t$ [MTh/GWh] | $\gamma_t$ [MTh/GWh] | $\theta_t$ [MTh/GWh] |
| NUC_ALM1  | 1                    | 0                   | 0                    | 0                    |
| NUC_ALM2  | 1                    | 0                   | 0                    | 0                    |
| NUC_ASC1  | 1                    | 0                   | 0                    | 0                    |
| NUC_ASC2  | 1                    | 0                   | 0                    | 0                    |
| NUC_COF   | 1                    | 0                   | 0                    | 0                    |
| NUC_GAR   | 1                    | 0                   | 0                    | 0                    |
| NUC_TRI   | 1                    | 0                   | 0                    | 0                    |
| NUC_VAN2  | 1                    | 0                   | 0                    | 0                    |
| COAL_ABO1   | 2.6                  | 0.05                | 2                    | 0.2                  |
| COAL_ABO2   | 2.6                  | 0.07                | 3.177                | 0.318                |
| COAL_ANL  | 2.6                  | 0.05                | 2.086                | 0.209                |
| COAL_COM2   | 2.6                  | 0.02                | 0.806                | 0.081                |
| COAL_COM3   | 2.6                  | 0.04                | 1.886                | 0.189                |
| COAL_COM4   | 2.6                  | 0.04                | 2                    | 0.2                  |
| COAL_COM5   | 2.6                  | 0.04                | 2                    | 0.2                  |
| COAL_GUA1   | 2.6                  | 0.02                | 0.886                | 0.089                |
| COAL_GUA2   | 2.6                  | 0.05                | 2.063                | 0.206                |
| COAL_LRO1   | 2.6                  | 0.04                | 1.623                | 0.162                |
| COAL_LRO2   | 2.6                  | 0.05                | 2.12                 | 0.212                |
| COAL_LAD4   | 2.6                  | 0.05                | 2.046                | 0.205                |
| COAL_LIT1   | 2.6                  | 0.07                | 3.297                | 0.33                 |
| COAL_LIT2   | 2.6                  | 0.07                | 3.326                | 0.333                |
| COAL_LBA  | 2.6                  | 0.08                | 3.366                | 0.337                |
| COAL_MEI  | 2.6                  | 0.07                | 3.217                | 0.322                |
| COAL_NAR1   | 2.6                  | 0.01                | 0.371                | 0.037                |
| COAL_NAR2   | 2.6                  | 0.02                | 0.949                | 0.095                |
| COAL_NAR3   | 2.6                  | 0.05                | 2.08                 | 0.208                |
| COAL_PNU3   | 2.6                  | 0.04                | 1.851                | 0.185                |
| COAL_PUE1   | 2.6                  | 0.05                | 2.109                | 0.211                |
| COAL_PUE2   | 2.6                  | 0.05                | 2.091                | 0.209                |

| PARAMETERS OF THERMAL UNITS $\alpha_t, \beta_t, \gamma_t, \theta_t$ |                      |                     |                      |                      |
|---|----------------------|---------------------|----------------------|----------------------|
| UNIT  | $\alpha_t$ [MTh/GWh] | $\beta_t$ [MTh/GWh] | $\gamma_t$ [MTh/GWh] | $\theta_t$ [MTh/GWh] |
| COAL_PUE3   | 2.60                 | 0.05                | 2.091                | 0.209                |
| COAL_PUE4   | 2.60                 | 0.05                | 2.097                | 0.21                 |
| COAL_PLL  | 2.60                 | 0.03                | 1.263                | 0.126                |
| COAL_SOT2   | 2.60                 | 0.03                | 1.451                | 0.145                |
| COAL_SOT3   | 2.60                 | 0.04                | 2                    | 0.2                  |
| COAL_TER1   | 2.60                 | 0.05                | 2.103                | 0.21                 |
| COAL_TER2   | 2.60                 | 0.05                | 2.103                | 0.21                 |
| COAL_TER3   | 2.60                 | 0.05                | 2.091                | 0.209                |
| CCGT_ACE3   | 1.30                 | 0.08                | 1.1                  | 0.11                 |
| CCGT_ACE4   | 1.30                 | 0.075               | 1.1                  | 0.11                 |
| CCGT_ALG3   | 1.30                 | 0.164               | 2.2                  | 0.2                  |
| CCGT_AMO  | 1.30                 | 0.15                | 1.1                  | 0.11                 |
| CCGT_ARC1   | 1.30                 | 0.079               | 1.1                  | 0.11                 |
| CCGT_ARC2   | 1.30                 | 0.076               | 1.1                  | 0.11                 |
| CCGT_ARC3   | 1.30                 | 0.169               | 2.2                  | 0.2                  |
| CCGT_ARR1   | 1.30                 | 0.08                | 1.1                  | 0.11                 |
| CCGT_ARR2   | 1.30                 | 0.079               | 1.1                  | 0.11                 |
| CCGT_BIZ  | 1.30                 | 0.16                | 2.2                  | 0.2                  |
| CCGT_BES3   | 1.30                 | 0.082               | 1.1                  | 0.11                 |
| CCGT_BES4   | 1.30                 | 0.081               | 1.1                  | 0.11                 |
| CCGT_BES5   | 1.30                 | 0.175               | 2.2                  | 0.2                  |
| CCGT_GIB1   | 1.30                 | 0.079               | 1.1                  | 0.11                 |
| CCGT_GIB2   | 1.30                 | 0.078               | 1.1                  | 0.11                 |
| CCGT_CAR1   | 1.30                 | 0.085               | 1.1                  | 0.11                 |
| CCGT_CAR2   | 1.30                 | 0.085               | 1.1                  | 0.11                 |
| CCGT_CAR3   | 1.30                 | 0.084               | 1.1                  | 0.11                 |
| CCGT_CJN1   | 1.30                 | 0.086               | 1.1                  | 0.11                 |
| CCGT_CJN2   | 1.30                 | 0.076               | 1.1                  | 0.11                 |
| CCGT_CJN3   | 1.30                 | 0.085               | 1.1                  | 0.11                 |
| CCGT_CLN3   | 1.30                 | 0.16                | 2.2                  | 0.2                  |
| CCGT_CLN4   | 1.30                 | 0.171               | 2.2                  | 0.2                  |
| CCGT_CNO  | 1.30                 | 0.16                | 2.2                  | 0.2                  |

| PARAMETERS OF THERMAL UNITS $\alpha_t, \beta_t, \gamma_t, \theta_t$ |                      |                     |                      |                      |
|---|----------------------|---------------------|----------------------|----------------------|
| UNIT  | $\alpha_t$ [MTh/GWh] | $\beta_t$ [MTh/GWh] | $\gamma_t$ [MTh/GWh] | $\theta_t$ [MTh/GWh] |
| CCGT_COL4   | 1.30                 | 0.08                | 1.1                  | 0.11                 |
| CCGT_EFG1   | 1.30                 | 0.082               | 1.1                  | 0.11                 |
| CCGT_EFG2   | 1.30                 | 0.082               | 1.1                  | 0.11                 |
| CCGT_EFG3   | 1.30                 | 0.08                | 1.1                  | 0.11                 |
| CCGT_ESC3   | 1.30                 | 0.164               | 2.2                  | 0.2                  |
| CCGT_ESCP   | 1.30                 | 0.057               | 1.1                  | 0.11                 |
| CCGT_ESC6   | 1.30                 | 0.166               | 2.2                  | 0.2                  |
| CCGT_MAL1   | 1.30                 | 0.088               | 1.1                  | 0.11                 |
| CCGT_PAL1   | 1.30                 | 0.08                | 1.1                  | 0.11                 |
| CCGT_PAL2   | 1.30                 | 0.079               | 1.1                  | 0.11                 |
| CCGT_PAL3   | 1.30                 | 0.08                | 1.1                  | 0.11                 |
| CCGT_PLV1   | 1.30                 | 0.082               | 1.1                  | 0.11                 |
| CCGT_PLV2   | 1.30                 | 0.084               | 1.1                  | 0.11                 |
| CCGT_PUE  | 1.30                 | 0.17                | 2.2                  | 0.2                  |
| CCGT_PUB1   | 1.30                 | 0.083               | 1.1                  | 0.11                 |
| CCGT_PUB2   | 1.30                 | 0.087               | 1.1                  | 0.11                 |
| CCGT_SAB3   | 1.30                 | 0.078               | 1.1                  | 0.11                 |
| CCGT_SAG1   | 1.30                 | 0.083               | 1.1                  | 0.11                 |
| CCGT_SAG2   | 1.30                 | 0.084               | 1.1                  | 0.11                 |
| CCGT_SAG3   | 1.30                 | 0.084               | 1.1                  | 0.11                 |
| CCGT_SRO1   | 1.30                 | 0.079               | 1.1                  | 0.11                 |
| CCGT_SRO2   | 1.30                 | 0.08                | 1.1                  | 0.11                 |
| CCGT_STU4   | 1.30                 | 0.081               | 1.1                  | 0.11                 |
| CCGT_RIB4   | 1.30                 | 0.086               | 1.1                  | 0.11                 |
| CCGT_RIB5   | 1.30                 | 0.087               | 1.1                  | 0.11                 |
| CCGT_TARE   | 1.30                 | 0.08                | 1.1                  | 0.11                 |
| CCGT_TARP   | 1.3                  | 0.085               | 1.1                  | 0.11                 |
| GAS_ECG   | 1.30                 | 0.086               | 1.1                  | 0.11                 |

**ANNEX C**  
**DEMAND LOAD LEVELS**



## ANNEX C DEMAND LOAD LEVELS

| YEAR 2015 - DEMAND [GW] |                       |         |         |         |         |         |         |         |         |
|-------------------------|-----------------------|---------|---------|---------|---------|---------|---------|---------|---------|
| Period                  | Sub-period/Load level |         |         |         |         |         |         |         |         |
| Week                    | lab.n1                | lab.n2  | lab.n3  | lab.n4  | lab.n5  | fes.n1  | fes.n2  | fes.n3  | fes.n4  |
| 1                       | 34.5452               | 32.9853 | 29.6330 | 23.6237 | 20.7176 | 30.0291 | 25.9489 | 22.3809 | 20.4702 |
| 2                       | 37.2465               | 35.8765 | 32.9024 | 26.1437 | 23.1620 | 31.1755 | 26.6830 | 23.4309 | 21.3743 |
| 3                       | 38.2171               | 36.9186 | 34.1497 | 26.9756 | 23.9881 | 32.8313 | 28.8396 | 24.2146 | 22.2518 |
| 4                       | 39.2300               | 37.6239 | 34.6345 | 27.5937 | 24.4096 | 32.2786 | 27.9453 | 24.3270 | 22.3614 |
| 5                       | 38.9528               | 37.1718 | 34.3491 | 27.4735 | 24.3351 | 32.9656 | 28.5962 | 24.6422 | 22.6583 |
| 6                       | 39.4340               | 37.5301 | 34.6243 | 27.6200 | 24.6749 | 32.7507 | 29.0378 | 24.2142 | 22.1011 |
| 7                       | 39.3819               | 37.2507 | 34.0948 | 27.7642 | 24.3032 | 31.6793 | 27.7612 | 24.2407 | 22.5668 |
| 8                       | 37.7440               | 36.1343 | 33.3506 | 27.1569 | 24.1389 | 31.5948 | 27.4026 | 24.1348 | 22.1663 |
| 9                       | 37.6809               | 35.9752 | 33.2972 | 27.2347 | 24.1590 | 32.1607 | 27.7017 | 24.0902 | 22.2634 |
| 10                      | 37.0689               | 35.0977 | 32.1579 | 26.4547 | 23.6848 | 29.6879 | 25.7767 | 23.3375 | 21.1636 |
| 11                      | 35.7271               | 34.1607 | 31.3721 | 25.7049 | 22.9049 | 29.6156 | 25.6522 | 23.0792 | 21.1416 |
| 12                      | 34.0673               | 32.2579 | 29.7099 | 24.7948 | 22.4701 | 29.0881 | 25.4665 | 22.4639 | 20.8345 |
| 13                      | 35.9986               | 34.2994 | 31.5584 | 25.8216 | 23.1936 | 30.6047 | 26.7674 | 23.4965 | 21.6207 |
| 14                      | 35.1993               | 33.7948 | 31.1346 | 25.8352 | 23.0298 | 28.8847 | 25.3503 | 22.9526 | 20.7642 |
| 15                      | 32.9320               | 31.6649 | 29.4544 | 24.8234 | 22.2119 | 27.7678 | 24.4167 | 22.3417 | 20.4477 |
| 16                      | 31.9494               | 30.4694 | 28.2409 | 23.9550 | 21.6800 | 25.3555 | 22.6594 | 20.6690 | 19.0953 |
| 17                      | 32.3297               | 30.5089 | 27.5123 | 23.4400 | 20.8816 | 27.9566 | 24.4826 | 22.1923 | 20.4968 |
| 18                      | 31.9391               | 30.4909 | 27.7034 | 23.4917 | 21.1092 | 26.1039 | 23.5155 | 21.1873 | 20.0248 |
| 19                      | 32.5063               | 31.3506 | 29.4272 | 24.7174 | 22.2949 | 27.9880 | 25.0341 | 22.3480 | 20.6991 |
| 20                      | 32.6573               | 31.3176 | 29.3384 | 24.8052 | 22.6582 | 27.2120 | 24.3278 | 21.8322 | 19.8998 |
| 21                      | 32.6856               | 31.3594 | 29.3205 | 24.8021 | 22.5327 | 27.4458 | 24.1501 | 22.0593 | 20.1494 |
| 22                      | 32.5897               | 31.2694 | 29.3171 | 24.7563 | 22.5189 | 27.2485 | 24.3394 | 21.6800 | 20.0358 |
| 23                      | 33.1493               | 31.5772 | 29.7203 | 24.9303 | 22.6162 | 28.1972 | 25.4063 | 22.9296 | 20.9413 |
| 24                      | 35.1702               | 33.3159 | 30.4913 | 25.5358 | 23.3593 | 29.9334 | 26.4598 | 23.6875 | 21.6441 |
| 25                      | 34.1767               | 32.5264 | 30.3935 | 25.9460 | 23.8729 | 28.7721 | 25.9676 | 23.4150 | 21.5134 |
| 26                      | 33.8272               | 31.9582 | 29.3094 | 25.3540 | 23.2516 | 29.3183 | 25.8959 | 23.3683 | 21.3269 |
| 27                      | 34.1855               | 32.3521 | 30.2350 | 25.9069 | 23.7328 | 28.9989 | 26.2018 | 23.0571 | 21.3513 |
| 28                      | 34.0332               | 32.6469 | 30.5291 | 26.1256 | 23.8519 | 28.6468 | 25.8630 | 23.5030 | 21.4551 |
| 29                      | 37.5542               | 35.7433 | 32.5430 | 27.2979 | 24.6924 | 29.7831 | 26.4963 | 24.0662 | 21.9298 |

## YEAR 2015 - DEMAND [GW]

| Period | Sub-period/Load level |         |         |         |         |         |         |         |         |
|--------|-----------------------|---------|---------|---------|---------|---------|---------|---------|---------|
|        | lab.n1                | lab.n2  | lab.n3  | lab.n4  | lab.n5  | fes.n1  | fes.n2  | fes.n3  | fes.n4  |
| 30     | 36.1703               | 34.5282 | 31.7458 | 26.8809 | 24.4190 | 30.2627 | 27.2262 | 24.0582 | 22.2416 |
| 31     | 35.2802               | 33.5425 | 30.7778 | 26.1104 | 23.8459 | 28.3263 | 25.6280 | 22.8328 | 21.0340 |
| 32     | 35.0417               | 33.2939 | 30.5174 | 25.2977 | 22.9537 | 29.5905 | 26.5951 | 23.5593 | 21.7753 |
| 33     | 33.9321               | 32.2330 | 27.6811 | 24.4010 | 22.3745 | 27.0989 | 24.9623 | 21.9711 | 20.7825 |
| 34     | 33.0387               | 31.7339 | 29.1854 | 24.8012 | 22.6158 | 27.9875 | 25.2547 | 22.2165 | 20.8712 |
| 35     | 37.0748               | 35.3317 | 32.0277 | 26.7242 | 24.0155 | 30.3557 | 27.2420 | 24.0436 | 22.2695 |
| 36     | 37.9203               | 36.5604 | 33.1203 | 27.6069 | 25.0404 | 30.7792 | 27.4597 | 24.3928 | 22.5003 |
| 37     | 36.3330               | 34.7027 | 31.6604 | 26.6389 | 24.2702 | 30.1699 | 26.7197 | 23.7219 | 22.0996 |
| 38     | 35.3026               | 34.0381 | 31.4139 | 25.9773 | 23.7309 | 28.9513 | 25.6379 | 23.1318 | 20.9027 |
| 39     | 33.4333               | 31.9325 | 29.5624 | 24.5044 | 22.4152 | 27.4687 | 24.3472 | 21.8126 | 20.1482 |
| 40     | 33.6555               | 32.3121 | 29.9754 | 24.5249 | 22.2965 | 27.9635 | 24.4977 | 21.9699 | 20.3675 |
| 41     | 33.5105               | 31.9356 | 29.5883 | 24.5031 | 22.2970 | 27.5032 | 24.2018 | 21.8423 | 20.1923 |
| 42     | 33.4110               | 31.7498 | 29.0281 | 24.0704 | 21.7192 | 27.8640 | 24.4174 | 21.8537 | 20.1469 |
| 43     | 33.7265               | 31.9547 | 29.6437 | 24.1850 | 21.9189 | 27.3581 | 24.0568 | 21.3017 | 19.3918 |
| 44     | 33.5065               | 31.7602 | 29.0849 | 23.8924 | 21.6520 | 26.6021 | 23.5922 | 20.8936 | 19.3133 |
| 45     | 34.4605               | 32.8426 | 29.9350 | 24.3405 | 21.9268 | 29.2538 | 25.5234 | 22.0512 | 20.3523 |
| 46     | 35.9418               | 34.2853 | 31.2782 | 25.4005 | 22.6800 | 29.7398 | 25.8139 | 22.8713 | 21.1709 |
| 47     | 36.4185               | 34.5009 | 31.7837 | 25.5738 | 23.0987 | 29.4692 | 26.1567 | 22.5124 | 20.8580 |
| 48     | 35.7311               | 34.2387 | 31.4242 | 25.1273 | 22.6796 | 30.0556 | 26.5163 | 22.3957 | 20.6555 |
| 49     | 36.4054               | 34.7427 | 32.1769 | 25.6854 | 22.8680 | 31.0548 | 27.4835 | 23.4134 | 22.1410 |
| 50     | 38.8752               | 36.9301 | 34.3246 | 27.1593 | 23.9217 | 32.4288 | 28.4152 | 24.0089 | 21.8559 |
| 51     | 38.2337               | 36.4031 | 33.5678 | 26.7970 | 23.7283 | 31.6349 | 27.7336 | 23.4343 | 21.7536 |
| 52     | 35.4811               | 33.1674 | 29.0553 | 23.7813 | 21.2035 | 30.0245 | 25.4272 | 21.4483 | 19.7528 |

## YEAR 2020 - DEMAND [GW]

| Period | Sub-period/Load level |         |         |         |         |         |         |         |         |
|--------|-----------------------|---------|---------|---------|---------|---------|---------|---------|---------|
| Week   | lab.n1                | lab.n2  | lab.n3  | lab.n4  | lab.n5  | fes.n1  | fes.n2  | fes.n3  | fes.n4  |
| 1      | 38.1288               | 36.4071 | 32.707  | 26.0743 | 22.8668 | 33.1442 | 28.6407 | 24.7026 | 22.5937 |
| 2      | 41.1103               | 39.5982 | 36.3156 | 28.8557 | 25.5647 | 34.4095 | 29.451  | 25.8615 | 23.5916 |
| 3      | 42.1816               | 40.7484 | 37.6923 | 29.7739 | 26.4765 | 36.2371 | 31.8313 | 26.7265 | 24.5601 |
| 4      | 43.2996               | 41.5269 | 38.2273 | 30.4562 | 26.9418 | 35.6271 | 30.8442 | 26.8506 | 24.6811 |
| 5      | 42.9936               | 41.0279 | 37.9123 | 30.3235 | 26.8595 | 36.3853 | 31.5627 | 27.1985 | 25.0088 |
| 6      | 43.5247               | 41.4233 | 38.2161 | 30.4852 | 27.2346 | 36.1481 | 32.0501 | 26.7261 | 24.3938 |
| 7      | 43.4672               | 41.1149 | 37.6317 | 30.6443 | 26.8243 | 34.9656 | 30.641  | 26.7553 | 24.9078 |
| 8      | 41.6594               | 39.8827 | 36.8103 | 29.9741 | 26.643  | 34.8723 | 30.2452 | 26.6384 | 24.4657 |
| 9      | 41.5898               | 39.7071 | 36.7513 | 30.0599 | 26.6652 | 35.4969 | 30.5754 | 26.5892 | 24.5729 |
| 10     | 40.9143               | 38.7386 | 35.4938 | 29.199  | 26.1418 | 32.7676 | 28.4507 | 25.7584 | 23.359  |
| 11     | 39.4333               | 37.7044 | 34.6265 | 28.3714 | 25.281  | 32.6878 | 28.3133 | 25.4733 | 23.3347 |
| 12     | 37.6013               | 35.6042 | 32.7919 | 27.3669 | 24.8011 | 32.1056 | 28.1083 | 24.7942 | 22.9958 |
| 13     | 39.733                | 37.8575 | 34.8321 | 28.5002 | 25.5996 | 33.7795 | 29.5441 | 25.9339 | 23.8635 |
| 14     | 38.8507               | 37.3005 | 34.3644 | 28.5152 | 25.4188 | 31.8811 | 27.98   | 25.3336 | 22.9182 |
| 15     | 36.3482               | 34.9497 | 32.5099 | 27.3985 | 24.5161 | 30.6483 | 26.9496 | 24.6593 | 22.5689 |
| 16     | 35.2637               | 33.6302 | 31.1705 | 26.44   | 23.929  | 27.9858 | 25.01   | 22.8131 | 21.0762 |
| 17     | 35.6835               | 33.6738 | 30.3663 | 25.8716 | 23.0478 | 30.8567 | 27.0223 | 24.4944 | 22.6231 |
| 18     | 35.2523               | 33.6539 | 30.5772 | 25.9286 | 23.299  | 28.8118 | 25.9549 | 23.3852 | 22.1021 |
| 19     | 35.8784               | 34.6028 | 32.4799 | 27.2815 | 24.6077 | 30.8914 | 27.631  | 24.6663 | 22.8463 |
| 20     | 36.045                | 34.5664 | 32.3819 | 27.3784 | 25.0087 | 30.0349 | 26.8515 | 24.097  | 21.9641 |
| 21     | 36.0763               | 34.6125 | 32.3621 | 27.375  | 24.8702 | 30.2929 | 26.6553 | 24.3476 | 22.2396 |
| 22     | 35.9704               | 34.5132 | 32.3583 | 27.3244 | 24.8549 | 30.0752 | 26.8643 | 23.929  | 22.1142 |
| 23     | 36.5881               | 34.8529 | 32.8034 | 27.5165 | 24.9623 | 31.1223 | 28.0419 | 25.3082 | 23.1137 |
| 24     | 38.8186               | 36.772  | 33.6543 | 28.1848 | 25.7825 | 33.0386 | 29.2046 | 26.1447 | 23.8894 |
| 25     | 37.7221               | 35.9006 | 33.5464 | 28.6375 | 26.3494 | 31.7568 | 28.6614 | 25.844  | 23.7451 |
| 26     | 37.3363               | 35.2734 | 32.3498 | 27.9841 | 25.6636 | 32.3597 | 28.5822 | 25.7924 | 23.5393 |
| 27     | 37.7318               | 35.7082 | 33.3715 | 28.5944 | 26.1947 | 32.0071 | 28.9199 | 25.449  | 23.5662 |
| 28     | 37.5637               | 36.0336 | 33.6961 | 28.8358 | 26.3262 | 31.6185 | 28.5459 | 25.9411 | 23.6808 |
| 29     | 41.4499               | 39.4512 | 35.9189 | 30.1297 | 27.2539 | 32.8727 | 29.2449 | 26.5627 | 24.2047 |
| 30     | 39.9225               | 38.11   | 35.039  | 29.6694 | 26.9521 | 33.402  | 30.0505 | 26.5539 | 24.5489 |
| 31     | 38.94                 | 37.0221 | 33.9706 | 28.819  | 26.3196 | 31.2648 | 28.2865 | 25.2014 | 23.216  |

## YEAR 2020 - DEMAND [GW]

| Period | Sub-period/Load level |         |         |         |         |         |         |         |         |
|--------|-----------------------|---------|---------|---------|---------|---------|---------|---------|---------|
| Week   | lab.n1                | lab.n2  | lab.n3  | lab.n4  | lab.n5  | fes.n1  | fes.n2  | fes.n3  | fes.n4  |
| 32     | 38.6768               | 36.7477 | 33.6832 | 27.922  | 25.3348 | 32.6601 | 29.354  | 26.0032 | 24.0342 |
| 33     | 37.4521               | 35.5767 | 30.5526 | 26.9323 | 24.6955 | 29.91   | 27.5518 | 24.2503 | 22.9384 |
| 34     | 36.466                | 35.0259 | 32.213  | 27.374  | 24.9619 | 30.8908 | 27.8745 | 24.5212 | 23.0363 |
| 35     | 40.9208               | 38.9969 | 35.3501 | 29.4965 | 26.5068 | 33.5047 | 30.068  | 26.5378 | 24.5797 |
| 36     | 41.854                | 40.353  | 36.5561 | 30.4707 | 27.638  | 33.9721 | 30.3083 | 26.9232 | 24.8344 |
| 37     | 40.102                | 38.3026 | 34.9447 | 29.4023 | 26.7879 | 33.2996 | 29.4915 | 26.1827 | 24.3921 |
| 38     | 38.9648               | 37.5691 | 34.6727 | 28.6721 | 26.1927 | 31.9546 | 28.2975 | 25.5314 | 23.0711 |
| 39     | 36.9015               | 35.2451 | 32.6291 | 27.0464 | 24.7405 | 30.3182 | 26.8729 | 24.0754 | 22.2383 |
| 40     | 37.1468               | 35.664  | 33.0849 | 27.069  | 24.6095 | 30.8643 | 27.039  | 24.249  | 22.4803 |
| 41     | 36.9867               | 35.2485 | 32.6577 | 27.045  | 24.61   | 30.3563 | 26.7124 | 24.1081 | 22.287  |
| 42     | 36.8769               | 35.0434 | 32.0394 | 26.5674 | 23.9723 | 30.7545 | 26.9504 | 24.1207 | 22.2369 |
| 43     | 37.2252               | 35.2696 | 32.7188 | 26.6939 | 24.1927 | 30.1961 | 26.5524 | 23.5115 | 21.4034 |
| 44     | 36.9823               | 35.0549 | 32.1021 | 26.3709 | 23.8981 | 29.3617 | 26.0396 | 23.061  | 21.3168 |
| 45     | 38.0353               | 36.2496 | 33.0403 | 26.8655 | 24.2014 | 32.2885 | 28.1711 | 24.3387 | 22.4636 |
| 46     | 39.6703               | 37.8419 | 34.5229 | 28.0354 | 25.0327 | 32.8249 | 28.4917 | 25.2439 | 23.3671 |
| 47     | 40.1964               | 38.0799 | 35.0808 | 28.2267 | 25.4949 | 32.5262 | 28.8701 | 24.8477 | 23.0217 |
| 48     | 39.4377               | 37.7905 | 34.684  | 27.7339 | 25.0323 | 33.1735 | 29.267  | 24.7189 | 22.7982 |
| 49     | 40.182                | 38.3468 | 35.5148 | 28.3499 | 25.2402 | 34.2763 | 30.3345 | 25.8422 | 24.4378 |
| 50     | 42.908                | 40.7611 | 37.8853 | 29.9767 | 26.4032 | 35.7928 | 31.3629 | 26.4995 | 24.1231 |
| 51     | 42.1999               | 40.1794 | 37.05   | 29.5768 | 26.1898 | 34.9166 | 30.6106 | 25.8653 | 24.0102 |
| 52     | 39.1618               | 36.6081 | 32.0694 | 26.2483 | 23.4031 | 33.1391 | 28.0649 | 23.6733 | 21.8019 |

**ANNEX D**

**PRODUCTION PATTERNS FOR RENEWABLE, COGENERATION  
AND WASTE-TO-ENERGY GENERATION**

## ANNEX D PRODUCTION PATTERNS FOR RENEWABLE, COGENERATION AND WASTE-TO-ENERGY GENERATION

### YEAR 2015 - WIND GENERATION [GW]

| Period | Sub-period /Load level |         |         |         |        |         |         |         |        |
|--------|------------------------|---------|---------|---------|--------|---------|---------|---------|--------|
| Week   | lab.n1                 | lab.n2  | lab.n3  | lab.n4  | lab.n5 | fes.n1  | fes.n2  | fes.n3  | fes.n4 |
| 1      | 9.3908                 | 8.9879  | 8.6936  | 8.9317  | 7.5715 | 13.4321 | 11.2770 | 9.1023  | 8.8776 |
| 2      | 4.2890                 | 4.5857  | 4.6825  | 4.7713  | 5.4899 | 3.2857  | 5.9807  | 4.3206  | 6.6320 |
| 3      | 10.4516                | 8.6004  | 9.3724  | 9.7309  | 8.5358 | 7.4147  | 7.2254  | 6.1153  | 4.7708 |
| 4      | 8.0285                 | 8.7578  | 9.1434  | 8.1105  | 8.2815 | 10.9999 | 9.9704  | 11.1952 | 7.3780 |
| 5      | 12.1362                | 10.3746 | 11.7281 | 10.7080 | 9.6822 | 10.4822 | 8.6327  | 9.7325  | 9.1962 |
| 6      | 10.6128                | 11.8136 | 12.0148 | 9.4704  | 7.8941 | 11.4422 | 7.9001  | 7.0186  | 4.6328 |
| 7      | 10.7704                | 11.1515 | 10.8645 | 8.5039  | 6.9078 | 4.3491  | 4.0088  | 3.8773  | 2.1357 |
| 8      | 6.8767                 | 6.2310  | 7.2670  | 5.7380  | 5.5314 | 6.0930  | 5.8677  | 6.2570  | 5.0720 |
| 9      | 8.7955                 | 8.7761  | 9.3583  | 8.4409  | 7.1745 | 11.5433 | 9.6407  | 8.3369  | 6.3468 |
| 10     | 12.8692                | 7.7979  | 7.2938  | 7.5149  | 6.2615 | 5.1306  | 5.0987  | 4.6800  | 5.1392 |
| 11     | 4.4879                 | 3.2413  | 4.1666  | 4.0472  | 3.8849 | 6.1157  | 5.8331  | 6.1882  | 7.5334 |
| 12     | 4.8542                 | 2.9578  | 3.7194  | 4.2673  | 3.4420 | 8.4345  | 8.7878  | 7.3404  | 8.9519 |
| 13     | 11.9749                | 9.5985  | 9.7611  | 9.4702  | 7.5087 | 8.7603  | 7.4352  | 7.7439  | 6.2191 |
| 14     | 8.3868                 | 7.8297  | 9.5270  | 7.6554  | 7.5279 | 6.4554  | 5.1083  | 6.5612  | 4.3780 |
| 15     | 4.0797                 | 4.1310  | 4.6649  | 4.2073  | 4.0052 | 5.1525  | 4.3943  | 4.9286  | 3.6856 |
| 16     | 2.5306                 | 1.6201  | 2.1472  | 2.5460  | 2.8681 | 3.7420  | 3.9087  | 3.9444  | 4.9774 |
| 17     | 8.8224                 | 7.5157  | 4.8662  | 5.2260  | 4.0580 | 10.1791 | 9.2218  | 9.8521  | 8.9654 |
| 18     | 3.7702                 | 4.4483  | 6.9703  | 4.7374  | 5.3652 | 5.6416  | 4.6317  | 6.2776  | 5.6540 |
| 19     | 2.0848                 | 2.5147  | 3.4886  | 3.4059  | 3.2962 | 2.9018  | 3.9875  | 2.1654  | 3.0560 |
| 20     | 5.9473                 | 7.0825  | 8.7400  | 8.0653  | 7.0500 | 7.2242  | 5.8011  | 7.2118  | 3.9761 |
| 21     | 9.2078                 | 9.1150  | 8.2047  | 8.0853  | 7.6958 | 3.2489  | 3.0655  | 1.9905  | 2.3780 |
| 22     | 3.4853                 | 4.0582  | 4.9011  | 3.2948  | 3.3193 | 6.0802  | 6.0300  | 6.0241  | 6.6523 |
| 23     | 7.2714                 | 5.2219  | 4.5901  | 4.2868  | 3.9323 | 6.3957  | 5.4180  | 6.1660  | 2.3997 |
| 24     | 2.9591                 | 2.9670  | 3.9174  | 3.2689  | 3.0510 | 9.0162  | 9.1858  | 8.1967  | 9.0243 |
| 25     | 3.0392                 | 3.7037  | 4.3070  | 5.1175  | 5.4839 | 2.6990  | 2.2839  | 1.6212  | 1.6497 |
| 26     | 1.8518                 | 3.1878  | 3.2350  | 2.9353  | 3.1985 | 7.4964  | 5.5496  | 4.7056  | 6.2771 |
| 27     | 3.3536                 | 4.6314  | 4.4016  | 4.0571  | 3.3928 | 5.6997  | 5.1675  | 4.8791  | 5.5948 |
| 28     | 6.3701                 | 7.0381  | 6.9635  | 6.6275  | 5.9155 | 4.5832  | 3.4080  | 4.5589  | 2.4977 |

## YEAR 2015 - WIND GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |         |         |         |         |
|--------|------------------------|--------|--------|--------|--------|---------|---------|---------|---------|
| Week   | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1  | fes.n2  | fes.n3  | fes.n4  |
| 29     | 4.5772                 | 4.7999 | 4.1503 | 3.7490 | 3.7213 | 7.2651  | 6.8901  | 5.3979  | 6.5830  |
| 30     | 1.3661                 | 3.0235 | 3.9356 | 3.9535 | 3.9416 | 3.4344  | 3.8657  | 4.0332  | 4.0801  |
| 31     | 3.8458                 | 4.5346 | 5.4592 | 5.0505 | 4.7860 | 4.3906  | 2.9191  | 4.5622  | 1.5884  |
| 32     | 1.9643                 | 2.5081 | 2.8679 | 2.7730 | 2.5559 | 4.4495  | 3.9329  | 2.9141  | 5.1249  |
| 33     | 3.3897                 | 4.8692 | 4.5289 | 4.4926 | 4.0957 | 5.5698  | 4.7767  | 5.1919  | 5.7041  |
| 34     | 2.4770                 | 3.4387 | 4.3888 | 4.0306 | 4.1619 | 2.3237  | 2.8904  | 3.5044  | 2.5376  |
| 35     | 3.1251                 | 4.1521 | 4.4821 | 3.9413 | 3.5335 | 3.8893  | 4.0589  | 4.4775  | 3.7318  |
| 36     | 1.5599                 | 2.0473 | 2.3818 | 2.8333 | 2.7732 | 2.0843  | 2.2628  | 1.3552  | 1.1028  |
| 37     | 1.0975                 | 1.7324 | 2.1596 | 2.1923 | 2.0128 | 1.5847  | 2.1400  | 1.1182  | 1.1151  |
| 38     | 5.6292                 | 5.9993 | 5.6445 | 5.1800 | 4.8416 | 2.3014  | 2.0149  | 2.2890  | 0.9415  |
| 39     | 3.2783                 | 3.0530 | 3.6516 | 3.9770 | 3.9362 | 3.0907  | 2.5477  | 2.8207  | 2.2207  |
| 40     | 3.6477                 | 2.0959 | 2.5171 | 3.2273 | 2.5210 | 2.2130  | 2.4792  | 2.5508  | 5.6299  |
| 41     | 6.2728                 | 5.3186 | 5.1123 | 5.9154 | 5.1359 | 4.3734  | 6.3148  | 3.7188  | 7.9618  |
| 42     | 8.0160                 | 7.3890 | 6.6320 | 7.4006 | 6.2962 | 6.3950  | 5.7857  | 6.5206  | 4.8610  |
| 43     | 4.9529                 | 4.3762 | 4.4914 | 5.6262 | 5.1656 | 2.6488  | 2.3742  | 2.6985  | 2.3985  |
| 44     | 3.3962                 | 3.5537 | 3.6905 | 3.8707 | 3.5365 | 2.6158  | 3.3698  | 2.5156  | 4.7633  |
| 45     | 9.4602                 | 9.0607 | 9.4599 | 9.5151 | 8.4891 | 7.0016  | 5.6159  | 4.9138  | 5.1229  |
| 46     | 10.3073                | 9.1528 | 9.0109 | 9.8199 | 8.4618 | 12.8410 | 12.5170 | 11.4703 | 11.6874 |
| 47     | 5.8468                 | 5.2329 | 5.5089 | 5.8565 | 6.4560 | 6.3095  | 7.2402  | 5.3805  | 9.2261  |
| 48     | 5.7260                 | 5.1953 | 4.7443 | 4.5725 | 4.8499 | 7.9867  | 8.9840  | 5.1931  | 8.2377  |
| 49     | 8.2355                 | 7.4260 | 8.7205 | 7.9297 | 8.0987 | 9.6139  | 9.4794  | 9.5986  | 10.0660 |
| 50     | 6.6226                 | 6.9526 | 6.7884 | 6.6990 | 7.8296 | 7.5222  | 6.6810  | 7.3285  | 6.1741  |
| 51     | 7.7121                 | 5.8477 | 5.2804 | 6.4685 | 6.3414 | 3.3528  | 3.1588  | 4.1688  | 4.2569  |
| 52     | 2.8995                 | 2.5764 | 2.6989 | 3.4481 | 3.5695 | 11.5046 | 7.6624  | 6.4823  | 5.1080  |

## YEAR 2020 - WIND GENERATION [GW]

| Period | Sub-period /Load level |         |         |         |         |         |         |         |         |
|--------|------------------------|---------|---------|---------|---------|---------|---------|---------|---------|
| Week   | lab.n1                 | lab.n2  | lab.n3  | lab.n4  | lab.n5  | fes.n1  | fes.n2  | fes.n3  | fes.n4  |
| 1      | 11.366                 | 10.8783 | 10.5221 | 10.8103 | 9.164   | 16.2573 | 13.6489 | 11.0168 | 10.7448 |
| 2      | 5.1911                 | 5.5502  | 5.6674  | 5.7748  | 6.6446  | 3.9768  | 7.2386  | 5.2294  | 8.0269  |
| 3      | 12.6499                | 10.4093 | 11.3437 | 11.7776 | 10.3311 | 8.9742  | 8.7451  | 7.4015  | 5.7742  |
| 4      | 9.7171                 | 10.5998 | 11.0665 | 9.8164  | 10.0234 | 13.3135 | 12.0675 | 13.5499 | 8.9298  |
| 5      | 14.6888                | 12.5567 | 14.1949 | 12.9602 | 11.7187 | 12.6869 | 10.4484 | 11.7795 | 11.1304 |
| 6      | 12.845                 | 14.2984 | 14.5419 | 11.4623 | 9.5545  | 13.8488 | 9.5617  | 8.4948  | 5.6072  |
| 7      | 13.0357                | 13.497  | 13.1496 | 10.2925 | 8.3607  | 5.2638  | 4.852   | 4.6928  | 2.5849  |
| 8      | 8.3231                 | 7.5416  | 8.7955  | 6.9449  | 6.6948  | 7.3745  | 7.1019  | 7.573   | 6.1388  |
| 9      | 10.6455                | 10.622  | 11.3266 | 10.2163 | 8.6835  | 13.9712 | 11.6684 | 10.0904 | 7.6817  |
| 10     | 15.576                 | 9.438   | 8.8279  | 9.0955  | 7.5785  | 6.2097  | 6.1711  | 5.6643  | 6.2201  |
| 11     | 5.4318                 | 3.923   | 5.043   | 4.8984  | 4.702   | 7.402   | 7.06    | 7.4898  | 9.1179  |
| 12     | 5.8752                 | 3.5799  | 4.5017  | 5.1648  | 4.166   | 10.2085 | 10.6361 | 8.8843  | 10.8348 |
| 13     | 14.4936                | 11.6174 | 11.8142 | 11.4621 | 9.088   | 10.6029 | 8.999   | 9.3727  | 7.5272  |
| 14     | 10.1508                | 9.4765  | 11.5308 | 9.2656  | 9.1112  | 7.8132  | 6.1827  | 7.9412  | 5.2988  |
| 15     | 4.9378                 | 4.9999  | 5.6461  | 5.0922  | 4.8476  | 6.2362  | 5.3186  | 5.9652  | 4.4608  |
| 16     | 3.0629                 | 1.9609  | 2.5988  | 3.0815  | 3.4713  | 4.5291  | 4.7308  | 4.774   | 6.0243  |
| 17     | 10.678                 | 9.0965  | 5.8897  | 6.3252  | 4.9115  | 12.3201 | 11.1614 | 11.9243 | 10.8511 |
| 18     | 4.5632                 | 5.3839  | 8.4364  | 5.7338  | 6.4937  | 6.8282  | 5.6059  | 7.598   | 6.8432  |
| 19     | 2.5233                 | 3.0436  | 4.2224  | 4.1223  | 3.9895  | 3.5121  | 4.8262  | 2.6208  | 3.6988  |
| 20     | 7.1982                 | 8.5722  | 10.5783 | 9.7617  | 8.5328  | 8.7437  | 7.0212  | 8.7287  | 4.8124  |
| 21     | 11.1445                | 11.0322 | 9.9304  | 9.7859  | 9.3145  | 3.9322  | 3.7103  | 2.4092  | 2.8782  |
| 22     | 4.2184                 | 4.9118  | 5.932   | 3.9878  | 4.0174  | 7.3591  | 7.2983  | 7.2912  | 8.0515  |
| 23     | 8.8008                 | 6.3202  | 5.5555  | 5.1884  | 4.7594  | 7.7409  | 6.5576  | 7.4629  | 2.9044  |
| 24     | 3.5815                 | 3.5911  | 4.7413  | 3.9564  | 3.6927  | 10.9126 | 11.1179 | 9.9207  | 10.9224 |
| 25     | 3.6784                 | 4.4827  | 5.2129  | 6.1939  | 6.6373  | 3.2667  | 2.7643  | 1.9622  | 1.9967  |
| 26     | 2.2413                 | 3.8583  | 3.9154  | 3.5527  | 3.8712  | 9.0731  | 6.7169  | 5.6953  | 7.5974  |
| 27     | 4.059                  | 5.6055  | 5.3274  | 4.9104  | 4.1064  | 6.8985  | 6.2544  | 5.9053  | 6.7716  |
| 28     | 7.7099                 | 8.5184  | 8.4281  | 8.0215  | 7.1597  | 5.5472  | 4.1248  | 5.5178  | 3.023   |
| 29     | 5.5399                 | 5.8095  | 5.0232  | 4.5375  | 4.504   | 8.7932  | 8.3393  | 6.5332  | 7.9676  |
| 30     | 1.6534                 | 3.6594  | 4.7634  | 4.785   | 4.7706  | 4.1568  | 4.6788  | 4.8815  | 4.9383  |
| 31     | 4.6547                 | 5.4884  | 6.6074  | 6.1128  | 5.7926  | 5.3141  | 3.5331  | 5.5218  | 1.9225  |



## YEAR 2020 - WIND GENERATION [GW]

| Period | Sub-period /Load level |         |         |         |         |         |         |         |         |
|--------|------------------------|---------|---------|---------|---------|---------|---------|---------|---------|
| Week   | lab.n1                 | lab.n2  | lab.n3  | lab.n4  | lab.n5  | fes.n1  | fes.n2  | fes.n3  | fes.n4  |
| 32     | 2.3775                 | 3.0356  | 3.4711  | 3.3562  | 3.0935  | 5.3854  | 4.7601  | 3.527   | 6.2028  |
| 33     | 4.1027                 | 5.8933  | 5.4815  | 5.4375  | 4.9572  | 6.7413  | 5.7814  | 6.2839  | 6.9038  |
| 34     | 2.998                  | 4.162   | 5.3119  | 4.8784  | 5.0373  | 2.8124  | 3.4983  | 4.2415  | 3.0713  |
| 35     | 3.7824                 | 5.0254  | 5.4248  | 4.7703  | 4.2767  | 4.7073  | 4.9126  | 5.4193  | 4.5167  |
| 36     | 1.888                  | 2.4779  | 2.8828  | 3.4292  | 3.3565  | 2.5227  | 2.7387  | 1.6402  | 1.3348  |
| 37     | 1.3283                 | 2.0968  | 2.6138  | 2.6534  | 2.4362  | 1.918   | 2.5901  | 1.3534  | 1.3496  |
| 38     | 6.8132                 | 7.2611  | 6.8317  | 6.2695  | 5.8599  | 2.7855  | 2.4387  | 2.7704  | 1.1395  |
| 39     | 3.9678                 | 3.6951  | 4.4196  | 4.8135  | 4.7641  | 3.7408  | 3.0836  | 3.414   | 2.6878  |
| 40     | 4.4149                 | 2.5367  | 3.0465  | 3.9061  | 3.0512  | 2.6785  | 3.0007  | 3.0873  | 6.814   |
| 41     | 7.5922                 | 6.4373  | 6.1876  | 7.1596  | 6.2161  | 5.2933  | 7.643   | 4.501   | 9.6364  |
| 42     | 9.702                  | 8.9431  | 8.0269  | 8.9572  | 7.6205  | 7.7401  | 7.0026  | 7.8921  | 5.8834  |
| 43     | 5.9946                 | 5.2966  | 5.4361  | 6.8096  | 6.2521  | 3.2059  | 2.8736  | 3.2661  | 2.903   |
| 44     | 4.1105                 | 4.3012  | 4.4667  | 4.6848  | 4.2803  | 3.166   | 4.0786  | 3.0447  | 5.7652  |
| 45     | 11.45                  | 10.9664 | 11.4496 | 11.5164 | 10.2746 | 8.4742  | 6.7971  | 5.9473  | 6.2004  |
| 46     | 12.4752                | 11.0779 | 10.9062 | 11.8853 | 10.2416 | 15.5419 | 15.1497 | 13.8829 | 14.1456 |
| 47     | 7.0766                 | 6.3335  | 6.6676  | 7.0883  | 7.8139  | 7.6366  | 8.763   | 6.5122  | 11.1666 |
| 48     | 6.9304                 | 6.288   | 5.7422  | 5.5342  | 5.87    | 9.6665  | 10.8736 | 6.2854  | 9.9703  |
| 49     | 9.9677                 | 8.9879  | 10.5547 | 9.5976  | 9.8021  | 11.636  | 11.4732 | 11.6175 | 12.1832 |
| 50     | 8.0155                 | 8.4149  | 8.2162  | 8.108   | 9.4764  | 9.1043  | 8.0862  | 8.8699  | 7.4727  |
| 51     | 9.3342                 | 7.0776  | 6.391   | 7.829   | 7.6752  | 4.058   | 3.8232  | 5.0456  | 5.1523  |
| 52     | 3.5094                 | 3.1183  | 3.2666  | 4.1733  | 4.3203  | 13.9244 | 9.274   | 7.8457  | 6.1824  |

## YEAR 2015 - SOLAR PHOTOVOLTAIC GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |        |        |        |        |
|--------|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 1      | 0.4926                 | 0.8287 | 0.5383 | 0.0000 | 0.0000 | 0.7177 | 0.4922 | 0.3502 | 0.1328 |
| 2      | 0.0000                 | 1.1228 | 0.4898 | 0.0000 | 0.0000 | 0.5517 | 0.7596 | 0.1731 | 0.0403 |
| 3      | 0.1904                 | 1.1412 | 0.4262 | 0.0000 | 0.0000 | 0.6326 | 0.7129 | 0.0633 | 0.0000 |
| 4      | 0.1506                 | 1.1652 | 0.4151 | 0.0000 | 0.0000 | 0.6326 | 0.7129 | 0.0000 | 0.0633 |
| 5      | 0.0000                 | 1.1045 | 0.5059 | 0.0000 | 0.0000 | 0.8635 | 0.9830 | 0.2151 | 0.1455 |
| 6      | 0.6819                 | 1.3031 | 0.8314 | 0.0000 | 0.0000 | 0.8635 | 1.0494 | 0.0253 | 0.1455 |
| 7      | 0.9963                 | 1.3284 | 0.7306 | 0.0000 | 0.0000 | 0.8635 | 0.9830 | 0.2151 | 0.1455 |
| 8      | 0.4694                 | 1.5764 | 0.6454 | 0.0000 | 0.0000 | 0.9710 | 0.9742 | 0.0253 | 0.1455 |
| 9      | 0.0000                 | 1.7472 | 0.6133 | 0.0000 | 0.0000 | 1.0975 | 1.1070 | 0.2657 | 0.2341 |
| 10     | 0.8236                 | 1.8167 | 0.7672 | 0.0000 | 0.0000 | 1.0975 | 1.0826 | 0.3353 | 0.2341 |
| 11     | 0.2435                 | 1.9787 | 0.7705 | 0.0000 | 0.0000 | 1.0975 | 1.1181 | 0.2341 | 0.2341 |
| 12     | 0.0000                 | 2.0521 | 0.7672 | 0.0000 | 0.0000 | 1.0975 | 1.1756 | 0.0696 | 0.2341 |
| 13     | 0.8635                 | 1.8256 | 0.7494 | 0.0000 | 0.0000 | 1.2304 | 0.9897 | 0.3353 | 0.2341 |
| 14     | 1.4745                 | 1.5384 | 1.2996 | 0.0000 | 0.0000 | 1.2398 | 1.4325 | 0.5377 | 0.0380 |
| 15     | 1.7933                 | 1.7168 | 1.1767 | 0.0000 | 0.0000 | 1.2398 | 1.4325 | 0.5377 | 0.0380 |
| 16     | 2.1992                 | 1.7923 | 1.0092 | 0.0000 | 0.0000 | 1.3974 | 1.5913 | 0.0915 | 0.0177 |
| 17     | 1.7933                 | 1.6877 | 1.1956 | 0.0177 | 0.0000 | 1.2398 | 1.5099 | 0.3163 | 0.0380 |
| 18     | 2.1199                 | 1.6478 | 1.3104 | 0.0480 | 0.0000 | 1.7177 | 1.8478 | 0.1650 | 0.0523 |
| 19     | 2.7808                 | 2.2848 | 1.1247 | 0.0000 | 0.0000 | 1.8123 | 1.6959 | 0.1771 | 0.0822 |
| 20     | 2.9446                 | 2.2254 | 1.1358 | 0.0000 | 0.0000 | 1.7522 | 1.7380 | 0.1771 | 0.0822 |
| 21     | 3.0465                 | 2.0710 | 1.2454 | 0.0000 | 0.0000 | 1.5783 | 1.7269 | 0.5567 | 0.0822 |
| 22     | 3.4140                 | 2.0344 | 1.1856 | 0.0000 | 0.0000 | 1.7680 | 1.7956 | 0.1961 | 0.1202 |
| 23     | 3.3918                 | 2.3721 | 1.1136 | 0.0089 | 0.0000 | 1.5719 | 2.0834 | 0.0190 | 0.1202 |
| 24     | 3.4228                 | 2.5025 | 0.9919 | 0.0089 | 0.0000 | 2.1507 | 1.6096 | 0.2151 | 0.1202 |
| 25     | 3.4096                 | 2.6935 | 0.8247 | 0.0177 | 0.0000 | 2.1001 | 1.6450 | 0.2151 | 0.1202 |
| 26     | 3.2811                 | 2.6138 | 0.9266 | 0.0177 | 0.0000 | 2.1507 | 1.6096 | 0.2151 | 0.1202 |
| 27     | 3.4007                 | 2.6707 | 1.1203 | 0.0089 | 0.0000 | 2.1286 | 1.8952 | 0.2214 | 0.1139 |
| 28     | 3.8524                 | 2.9301 | 0.8446 | 0.0177 | 0.0000 | 1.7048 | 2.1919 | 0.2214 | 0.1139 |
| 29     | 3.9144                 | 2.9490 | 0.8103 | 0.0236 | 0.0000 | 2.1792 | 1.8598 | 0.2214 | 0.1139 |
| 30     | 3.7461                 | 2.7732 | 1.0085 | 0.0177 | 0.0000 | 2.3405 | 1.7468 | 0.2214 | 0.1139 |
| 31     | 3.8169                 | 3.0376 | 0.6365 | 0.0118 | 0.0000 | 1.7111 | 1.7291 | 0.1581 | 0.0569 |

## YEAR 2015 - SOLAR PHOTOVOLTAIC GENERATION [GW]

| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 32     | 3.6398                | 2.3494 | 0.7871 | 0.0000 | 0.0000 | 1.9578 | 1.4612 | 0.4301 | 0.0569 |
| 33     | 3.5978                | 1.9736 | 1.0198 | 0.2509 | 0.0249 | 1.7343 | 1.7746 | 0.1731 | 0.0362 |
| 34     | 3.6221                | 2.2469 | 0.8812 | 0.0000 | 0.0000 | 1.9104 | 1.5897 | 0.1581 | 0.0569 |
| 35     | 3.5778                | 2.3418 | 0.8092 | 0.0000 | 0.0000 | 1.9578 | 1.5564 | 0.1581 | 0.0569 |
| 36     | 3.0066                | 2.2051 | 0.3410 | 0.0000 | 0.0000 | 1.6194 | 1.2443 | 0.1012 | 0.0127 |
| 37     | 2.7409                | 1.8964 | 0.6775 | 0.0000 | 0.0000 | 1.6194 | 1.2443 | 0.1012 | 0.0127 |
| 38     | 2.1299                | 1.9799 | 0.7572 | 0.0000 | 0.0000 | 1.4201 | 1.3838 | 0.1012 | 0.0127 |
| 39     | 1.4391                | 2.0242 | 0.8911 | 0.0000 | 0.0000 | 1.4518 | 1.3616 | 0.1012 | 0.0127 |
| 40     | 1.1734                | 1.5523 | 0.8756 | 0.0000 | 0.0000 | 0.9267 | 1.0959 | 0.0380 | 0.0000 |
| 41     | 0.8856                | 1.5106 | 0.6542 | 0.0000 | 0.0000 | 0.9267 | 1.0959 | 0.0380 | 0.0000 |
| 42     | 1.0627                | 1.1488 | 0.9266 | 0.0000 | 0.0000 | 0.9267 | 1.0959 | 0.0380 | 0.0000 |
| 43     | 0.7173                | 1.3018 | 0.8790 | 0.0000 | 0.0000 | 0.9077 | 1.1092 | 0.0380 | 0.0000 |
| 44     | 0.2834                | 1.4638 | 0.8457 | 0.0000 | 0.0000 | 0.6389 | 0.7328 | 0.0000 | 0.0696 |
| 45     | 0.0000                | 1.1778 | 0.4749 | 0.0000 | 0.0000 | 0.6389 | 0.7328 | 0.0000 | 0.0696 |
| 46     | 0.2037                | 1.1197 | 0.4749 | 0.0000 | 0.0000 | 0.5282 | 0.8103 | 0.0000 | 0.0696 |
| 47     | 0.0000                | 1.2221 | 0.4362 | 0.0000 | 0.0000 | 0.6389 | 0.7328 | 0.0000 | 0.0696 |
| 48     | 0.2037                | 1.1336 | 0.4627 | 0.0000 | 0.0000 | 0.6389 | 0.7328 | 0.0000 | 0.0696 |
| 49     | 0.0000                | 0.9210 | 0.5358 | 0.0000 | 0.0000 | 0.4681 | 0.6952 | 0.0506 | 0.0000 |
| 50     | 0.0000                | 0.9710 | 0.4511 | 0.0000 | 0.0000 | 0.4945 | 0.7170 | 0.0644 | 0.0000 |
| 51     | 0.0000                | 0.9223 | 0.4937 | 0.0000 | 0.0000 | 0.5662 | 0.5823 | 0.1771 | 0.0000 |
| 52     | 0.5535                | 0.6942 | 0.5549 | 0.0000 | 0.0000 | 0.5092 | 0.6216 | 0.2254 | 0.0322 |

## YEAR 2020 - SOLAR PHOTOVOLTAIC GENERATION [GW]

| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
|        | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 1      | 0.6441                | 1.0836 | 0.7039 | 0      | 0      | 0.9385 | 0.6436 | 0.4579 | 0.1736 |
| 2      | 0                     | 1.4682 | 0.6405 | 0      | 0      | 0.7214 | 0.9932 | 0.2263 | 0.0527 |
| 3      | 0.249                 | 1.4922 | 0.5573 | 0      | 0      | 0.8272 | 0.9322 | 0.0828 | 0      |
| 4      | 0.1969                | 1.5236 | 0.5428 | 0      | 0      | 0.8272 | 0.9322 | 0      | 0.0828 |
| 5      | 0                     | 1.4442 | 0.6615 | 0      | 0      | 1.1291 | 1.2854 | 0.2813 | 0.1903 |
| 6      | 0.8916                | 1.7039 | 1.0871 | 0      | 0      | 1.1291 | 1.3722 | 0.0331 | 0.1903 |
| 7      | 1.3028                | 1.737  | 0.9553 | 0      | 0      | 1.1291 | 1.2854 | 0.2813 | 0.1903 |
| 8      | 0.6138                | 2.0613 | 0.8439 | 0      | 0      | 1.2697 | 1.2739 | 0.0331 | 0.1903 |
| 9      | 0                     | 2.2846 | 0.8019 | 0      | 0      | 1.4351 | 1.4475 | 0.3474 | 0.3061 |
| 10     | 1.0769                | 2.3755 | 1.0032 | 0      | 0      | 1.4351 | 1.4156 | 0.4384 | 0.3061 |
| 11     | 0.3184                | 2.5873 | 1.0075 | 0      | 0      | 1.4351 | 1.462  | 0.3061 | 0.3061 |
| 12     | 0                     | 2.6833 | 1.0032 | 0      | 0      | 1.4351 | 1.5372 | 0.091  | 0.3061 |
| 13     | 1.1291                | 2.3871 | 0.9799 | 0      | 0      | 1.6089 | 1.2941 | 0.4384 | 0.3061 |
| 14     | 1.928                 | 2.0116 | 1.6993 | 0      | 0      | 1.6211 | 1.8731 | 0.7031 | 0.0497 |
| 15     | 2.3449                | 2.2449 | 1.5386 | 0      | 0      | 1.6211 | 1.8731 | 0.7031 | 0.0497 |
| 16     | 2.8756                | 2.3436 | 1.3196 | 0      | 0      | 1.8272 | 2.0808 | 0.1196 | 0.0231 |
| 17     | 2.3449                | 2.2068 | 1.5634 | 0.0231 | 0      | 1.6211 | 1.9743 | 0.4136 | 0.0497 |
| 18     | 2.772                 | 2.1546 | 1.7135 | 0.0628 | 0      | 2.246  | 2.4162 | 0.2158 | 0.0684 |
| 19     | 3.6361                | 2.9876 | 1.4706 | 0      | 0      | 2.3697 | 2.2175 | 0.2316 | 0.1075 |
| 20     | 3.8503                | 2.9099 | 1.4852 | 0      | 0      | 2.2912 | 2.2726 | 0.2316 | 0.1075 |
| 21     | 3.9836                | 2.708  | 1.6285 | 0      | 0      | 2.0638 | 2.2581 | 0.7279 | 0.1075 |
| 22     | 4.4641                | 2.6602 | 1.5503 | 0      | 0      | 2.3118 | 2.3479 | 0.2564 | 0.1572 |
| 23     | 4.4351                | 3.1017 | 1.4561 | 0.0116 | 0      | 2.0554 | 2.7242 | 0.0248 | 0.1572 |
| 24     | 4.4756                | 3.2722 | 1.297  | 0.0116 | 0      | 2.8122 | 2.1047 | 0.2813 | 0.1572 |
| 25     | 4.4584                | 3.522  | 1.0784 | 0.0231 | 0      | 2.7461 | 2.151  | 0.2813 | 0.1572 |
| 26     | 4.2903                | 3.4178 | 1.2116 | 0.0231 | 0      | 2.8122 | 2.1047 | 0.2813 | 0.1572 |
| 27     | 4.4467                | 3.4922 | 1.4649 | 0.0116 | 0      | 2.7833 | 2.4781 | 0.2895 | 0.1489 |
| 28     | 5.0374                | 3.8314 | 1.1044 | 0.0231 | 0      | 2.2292 | 2.8661 | 0.2895 | 0.1489 |
| 29     | 5.1184                | 3.8561 | 1.0595 | 0.0309 | 0      | 2.8495 | 2.4319 | 0.2895 | 0.1489 |
| 30     | 4.8984                | 3.6262 | 1.3187 | 0.0231 | 0      | 3.0604 | 2.2841 | 0.2895 | 0.1489 |
| 31     | 4.9909                | 3.9719 | 0.8323 | 0.0154 | 0      | 2.2374 | 2.261  | 0.2067 | 0.0744 |

## YEAR 2020 - SOLAR PHOTOVOLTAIC GENERATION [GW]

| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 32     | 4.7594                | 3.072  | 1.0292 | 0      | 0      | 2.56   | 1.9106 | 0.5624 | 0.0744 |
| 33     | 4.7044                | 2.5807 | 1.3335 | 0.3281 | 0.0326 | 2.2678 | 2.3204 | 0.2263 | 0.0473 |
| 34     | 4.7362                | 2.938  | 1.1522 | 0      | 0      | 2.498  | 2.0787 | 0.2067 | 0.0744 |
| 35     | 4.6783                | 3.0621 | 1.0581 | 0      | 0      | 2.56   | 2.0351 | 0.2067 | 0.0744 |
| 36     | 3.9314                | 2.8834 | 0.4459 | 0      | 0      | 2.1175 | 1.627  | 0.1323 | 0.0166 |
| 37     | 3.584                 | 2.4797 | 0.8859 | 0      | 0      | 2.1175 | 1.627  | 0.1323 | 0.0166 |
| 38     | 2.785                 | 2.5889 | 0.9901 | 0      | 0      | 1.8569 | 1.8094 | 0.1323 | 0.0166 |
| 39     | 1.8818                | 2.6468 | 1.1652 | 0      | 0      | 1.8984 | 1.7804 | 0.1323 | 0.0166 |
| 40     | 1.5343                | 2.0298 | 1.1449 | 0      | 0      | 1.2117 | 1.433  | 0.0497 | 0      |
| 41     | 1.158                 | 1.9752 | 0.8554 | 0      | 0      | 1.2117 | 1.433  | 0.0497 | 0      |
| 42     | 1.3896                | 1.5022 | 1.2116 | 0      | 0      | 1.2117 | 1.433  | 0.0497 | 0      |
| 43     | 0.9379                | 1.7022 | 1.1494 | 0      | 0      | 1.1869 | 1.4504 | 0.0497 | 0      |
| 44     | 0.3706                | 1.914  | 1.1058 | 0      | 0      | 0.8354 | 0.9582 | 0      | 0.091  |
| 45     | 0                     | 1.5401 | 0.621  | 0      | 0      | 0.8354 | 0.9582 | 0      | 0.091  |
| 46     | 0.2664                | 1.4641 | 0.621  | 0      | 0      | 0.6907 | 1.0595 | 0      | 0.091  |
| 47     | 0                     | 1.598  | 0.5704 | 0      | 0      | 0.8354 | 0.9582 | 0      | 0.091  |
| 48     | 0.2664                | 1.4823 | 0.605  | 0      | 0      | 0.8354 | 0.9582 | 0      | 0.091  |
| 49     | 0                     | 1.2043 | 0.7006 | 0      | 0      | 0.6121 | 0.909  | 0.0662 | 0      |
| 50     | 0                     | 1.2697 | 0.5899 | 0      | 0      | 0.6466 | 0.9375 | 0.0842 | 0      |
| 51     | 0                     | 1.206  | 0.6456 | 0      | 0      | 0.7404 | 0.7614 | 0.2316 | 0      |
| 52     | 0.7238                | 0.9077 | 0.7256 | 0      | 0      | 0.6658 | 0.8128 | 0.2947 | 0.0421 |

**YEAR 2015 AND YEAR 2020 - SOLAR THERMOELECTRIC GENERATION  
[GW]**

| <b>Period</b> | <b>Sub-period/Load level</b> |               |               |               |               |               |               |               |               |
|---------------|------------------------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| <b>Week</b>   | <b>lab.n1</b>                | <b>lab.n2</b> | <b>lab.n3</b> | <b>lab.n4</b> | <b>lab.n5</b> | <b>fes.n1</b> | <b>fes.n2</b> | <b>fes.n3</b> | <b>fes.n4</b> |
| 1             | 0.0159                       | 0.1048        | 0.1330        | 0.0053        | 0.0088        | 0.1035        | 0.0702        | 0.0070        | 0.0001        |
| 2             | 0.0397                       | 0.1605        | 0.2342        | 0.0088        | 0.0041        | 0.1848        | 0.1687        | 0.0457        | 0.0029        |
| 3             | 0.0261                       | 0.0635        | 0.0776        | 0.0085        | 0.0032        | 0.0391        | 0.1072        | 0.0016        | 0.0000        |
| 4             | 0.0281                       | 0.2726        | 0.3145        | 0.0035        | 0.0035        | 0.3548        | 0.3103        | 0.0000        | 0.0007        |
| 5             | 0.0113                       | 0.1725        | 0.2028        | 0.0029        | 0.0006        | 0.0827        | 0.3603        | 0.0101        | 0.0014        |
| 6             | 0.0566                       | 0.0840        | 0.0863        | 0.0021        | 0.0006        | 0.0405        | 0.0527        | 0.0000        | 0.0000        |
| 7             | 0.0367                       | 0.1088        | 0.1304        | 0.0024        | 0.0000        | 0.0865        | 0.3941        | 0.0140        | 0.0017        |
| 8             | 0.1235                       | 0.4071        | 0.3842        | 0.0198        | 0.0075        | 0.5375        | 0.4542        | 0.1161        | 0.0309        |
| 9             | 0.0456                       | 0.3184        | 0.2838        | 0.0224        | 0.0327        | 0.0045        | 0.0169        | 0.0024        | 0.0000        |
| 10            | 0.3054                       | 0.7262        | 0.7358        | 0.0995        | 0.0449        | 0.9772        | 0.5711        | 0.0913        | 0.0381        |
| 11            | 0.5675                       | 1.1803        | 1.0313        | 0.1533        | 0.1173        | 1.0804        | 1.0372        | 0.2762        | 0.0629        |
| 12            | 0.3661                       | 1.0101        | 0.8829        | 0.1440        | 0.1262        | 0.5228        | 1.0557        | 0.0096        | 0.0112        |
| 13            | 0.6811                       | 0.8171        | 0.5146        | 0.0951        | 0.0838        | 0.1412        | 0.3136        | 0.0038        | 0.0018        |
| 14            | 0.2773                       | 0.1981        | 0.2182        | 0.0310        | 0.0095        | 0.2571        | 0.6850        | 0.1859        | 0.0085        |
| 15            | 1.1174                       | 1.0997        | 0.9998        | 0.2622        | 0.3066        | 0.8992        | 1.0604        | 0.5540        | 0.0118        |
| 16            | 1.0075                       | 1.0993        | 0.7799        | 0.1981        | 0.1843        | 0.8139        | 0.8674        | 0.1487        | 0.1010        |
| 17            | 1.1544                       | 0.9489        | 0.4333        | 0.0512        | 0.0290        | 0.7889        | 0.9167        | 0.4122        | 0.1131        |
| 18            | 1.6051                       | 1.4242        | 1.2195        | 0.4179        | 0.5168        | 1.3836        | 1.6043        | 0.5314        | 0.3999        |
| 19            | 1.6278                       | 1.5892        | 1.0534        | 0.3635        | 0.4898        | 1.3159        | 1.2896        | 0.3995        | 0.1458        |
| 20            | 1.9490                       | 1.7485        | 1.1396        | 0.5151        | 0.5651        | 1.4207        | 1.4772        | 0.4060        | 0.2804        |
| 21            | 0.8920                       | 0.7873        | 0.5116        | 0.1082        | 0.2122        | 1.1257        | 1.2001        | 0.5016        | 0.1937        |
| 22            | 1.5095                       | 1.2818        | 0.9574        | 0.2987        | 0.2923        | 1.3368        | 1.3943        | 0.5384        | 0.3575        |
| 23            | 1.4828                       | 1.5912        | 1.0925        | 0.4076        | 0.4495        | 1.0272        | 1.5929        | 0.1573        | 0.2273        |
| 24            | 1.8072                       | 1.3630        | 0.7545        | 0.3181        | 0.3667        | 1.6778        | 1.3340        | 0.5708        | 0.3196        |
| 25            | 1.8491                       | 1.5620        | 0.7603        | 0.2811        | 0.3300        | 1.3037        | 1.0695        | 0.3604        | 0.2024        |
| 26            | 1.7628                       | 1.4636        | 0.5384        | 0.2189        | 0.1193        | 1.7532        | 1.4480        | 0.6794        | 0.5039        |
| 27            | 1.7981                       | 1.6096        | 0.9388        | 0.3334        | 0.3787        | 1.5466        | 1.0392        | 0.6101        | 0.2739        |
| 28            | 2.1231                       | 1.9943        | 1.0660        | 0.4958        | 0.4071        | 1.4874        | 1.7191        | 0.6884        | 0.5204        |
| 29            | 2.1056                       | 1.9726        | 1.0380        | 0.3873        | 0.5740        | 0.7707        | 1.2111        | 0.2273        | 0.0445        |
| 30            | 2.0844                       | 1.9468        | 1.0980        | 0.4303        | 0.4915        | 1.7551        | 1.4221        | 0.5789        | 0.4539        |

**YEAR 2015 AND YEAR 2020 - SOLAR THERMOELECTRIC GENERATION  
[GW]**

| <b>Period</b> | <b>Sub-period/Load level</b> |               |               |               |               |               |               |               |               |
|---------------|------------------------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|
| <b>Week</b>   | <b>lab.n1</b>                | <b>lab.n2</b> | <b>lab.n3</b> | <b>lab.n4</b> | <b>lab.n5</b> | <b>fes.n1</b> | <b>fes.n2</b> | <b>fes.n3</b> | <b>fes.n4</b> |
| 31            | 1.9786                       | 1.9190        | 0.9051        | 0.3928        | 0.5112        | 1.3132        | 1.3584        | 0.2557        | 0.1873        |
| 32            | 2.1021                       | 1.8948        | 1.0585        | 0.4562        | 0.5156        | 1.6164        | 1.3864        | 0.7955        | 0.3824        |
| 33            | 2.0991                       | 1.7512        | 1.0568        | 0.6508        | 0.5255        | 1.4774        | 1.6121        | 0.5102        | 0.4233        |
| 34            | 2.0444                       | 1.7081        | 1.0200        | 0.3137        | 0.4441        | 1.4942        | 1.4736        | 0.4885        | 0.3729        |
| 35            | 2.0042                       | 1.7732        | 0.9614        | 0.4302        | 0.5115        | 1.3569        | 1.2664        | 0.3522        | 0.1323        |
| 36            | 1.9611                       | 1.7586        | 0.6867        | 0.2861        | 0.2980        | 1.1447        | 0.6160        | 0.2682        | 0.0825        |
| 37            | 1.6972                       | 1.3584        | 0.6195        | 0.1658        | 0.1304        | 1.1785        | 1.0372        | 0.1794        | 0.0350        |
| 38            | 0.7167                       | 0.6963        | 0.3376        | 0.0816        | 0.0883        | 0.4069        | 0.3198        | 0.0164        | 0.0116        |
| 39            | 0.4554                       | 0.7897        | 0.4768        | 0.0542        | 0.0257        | 0.3432        | 0.3815        | 0.0329        | 0.0163        |
| 40            | 0.7075                       | 0.8291        | 0.5068        | 0.0241        | 0.0054        | 0.6520        | 0.7453        | 0.0423        | 0.0207        |
| 41            | 0.5987                       | 0.6738        | 0.3549        | 0.0581        | 0.0277        | 0.0935        | 0.1993        | 0.0101        | 0.0015        |
| 42            | 0.4567                       | 0.4266        | 0.2359        | 0.0250        | 0.0092        | 0.7446        | 0.6774        | 0.0290        | 0.0129        |
| 43            | 0.6101                       | 0.8162        | 0.6612        | 0.0167        | 0.0158        | 0.6687        | 0.5398        | 0.0593        | 0.0197        |
| 44            | 0.3647                       | 0.8139        | 0.6200        | 0.0159        | 0.0095        | 0.3954        | 0.5121        | 0.0114        | 0.0000        |
| 45            | 0.1440                       | 0.5202        | 0.4006        | 0.0129        | 0.0070        | 0.2198        | 0.3314        | 0.0000        | 0.0003        |
| 46            | 0.0277                       | 0.1365        | 0.1444        | 0.0065        | 0.0036        | 0.1611        | 0.3461        | 0.0094        | 0.0007        |
| 47            | 0.0400                       | 0.3532        | 0.3059        | 0.0025        | 0.0020        | 0.0300        | 0.0458        | 0.0000        | 0.0000        |
| 48            | 0.0234                       | 0.0590        | 0.0526        | 0.0037        | 0.0019        | 0.1046        | 0.1118        | 0.0044        | 0.0007        |
| 49            | 0.0316                       | 0.2146        | 0.2436        | 0.0009        | 0.0003        | 0.3085        | 0.4727        | 0.0066        | 0.0056        |
| 50            | 0.0385                       | 0.3557        | 0.3852        | 0.0057        | 0.0044        | 0.0557        | 0.2889        | 0.0026        | 0.0040        |
| 51            | 0.0172                       | 0.1789        | 0.3463        | 0.0017        | 0.0031        | 0.1502        | 0.2945        | 0.0008        | 0.0000        |
| 52            | 0.0958                       | 0.3523        | 0.3407        | 0.0006        | 0.0000        | 0.2580        | 0.1889        | 0.1757        | 0.0000        |

## YEAR 2015 – SMALL HYDRO GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |        |        |        |        |
|--------|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 1      | 0.9760                 | 0.9850 | 0.9677 | 0.8642 | 0.8321 | 0.9748 | 0.8834 | 0.7956 | 0.7968 |
| 2      | 1.0824                 | 1.0374 | 1.0502 | 0.9719 | 0.9280 | 1.0481 | 0.9846 | 0.9673 | 0.8705 |
| 3      | 1.0308                 | 1.0436 | 1.0183 | 0.9561 | 0.9520 | 1.0400 | 1.0089 | 0.9952 | 0.9905 |
| 4      | 1.1245                 | 1.1073 | 1.0890 | 1.0399 | 1.0123 | 1.0717 | 0.9882 | 0.9480 | 0.9385 |
| 5      | 1.1311                 | 1.1095 | 1.0726 | 0.9862 | 0.9274 | 1.0526 | 1.0361 | 0.9811 | 1.0155 |
| 6      | 1.1196                 | 1.1071 | 1.0738 | 0.9581 | 0.9396 | 0.9534 | 0.8917 | 0.8087 | 0.7374 |
| 7      | 1.0867                 | 1.0665 | 1.0361 | 0.8985 | 0.7728 | 1.1724 | 1.1053 | 0.9158 | 0.9964 |
| 8      | 1.1584                 | 1.1515 | 1.1073 | 1.0547 | 0.9804 | 1.1394 | 1.0334 | 1.0438 | 1.0205 |
| 9      | 1.1852                 | 1.1221 | 1.1056 | 1.0019 | 0.9622 | 1.0568 | 0.9598 | 0.9202 | 0.8137 |
| 10     | 1.0968                 | 1.0879 | 1.0733 | 0.9455 | 0.8774 | 1.1831 | 1.0168 | 0.9529 | 0.8039 |
| 11     | 1.2103                 | 1.1866 | 1.1627 | 1.0320 | 1.0130 | 1.0177 | 0.9707 | 0.9632 | 0.9017 |
| 12     | 1.1172                 | 1.0759 | 1.0269 | 0.9293 | 0.9086 | 0.9604 | 0.9686 | 0.8453 | 0.9340 |
| 13     | 1.0122                 | 0.9860 | 0.9536 | 0.8899 | 0.8809 | 0.9663 | 0.9333 | 0.9019 | 0.8949 |
| 14     | 1.1871                 | 1.1244 | 1.0925 | 1.0332 | 0.9775 | 1.1741 | 1.1220 | 1.0766 | 1.0579 |
| 15     | 1.2009                 | 1.1914 | 1.1694 | 1.1530 | 1.0778 | 1.1675 | 1.0617 | 1.0286 | 1.0022 |
| 16     | 1.1520                 | 1.1300 | 1.0921 | 1.0132 | 0.9623 | 0.9779 | 0.9304 | 0.9595 | 0.8940 |
| 17     | 0.9632                 | 0.9419 | 0.9448 | 0.9120 | 0.8816 | 1.0393 | 0.8839 | 0.8803 | 0.8089 |
| 18     | 1.0527                 | 1.0021 | 0.9709 | 0.9519 | 0.9266 | 0.9252 | 0.8957 | 0.8884 | 0.8873 |
| 19     | 0.9079                 | 0.8965 | 0.8739 | 0.8080 | 0.7997 | 0.8600 | 0.7926 | 0.7544 | 0.7582 |
| 20     | 0.8060                 | 0.7977 | 0.7819 | 0.7301 | 0.7106 | 0.7153 | 0.7031 | 0.6956 | 0.6824 |
| 21     | 0.7758                 | 0.7631 | 0.7588 | 0.6743 | 0.6536 | 0.7741 | 0.7312 | 0.7458 | 0.6808 |
| 22     | 0.8834                 | 0.8657 | 0.8252 | 0.7767 | 0.7277 | 0.7722 | 0.7591 | 0.7301 | 0.6977 |
| 23     | 0.7351                 | 0.7638 | 0.7476 | 0.7147 | 0.6870 | 0.7895 | 0.7896 | 0.7033 | 0.7901 |
| 24     | 0.8482                 | 0.8150 | 0.7771 | 0.7056 | 0.6810 | 0.7018 | 0.6765 | 0.6411 | 0.6218 |
| 25     | 0.8117                 | 0.7461 | 0.6774 | 0.5943 | 0.5871 | 0.6659 | 0.6576 | 0.5713 | 0.5775 |
| 26     | 0.8285                 | 0.7862 | 0.7368 | 0.6814 | 0.6356 | 0.7004 | 0.6829 | 0.6560 | 0.6266 |
| 27     | 0.7433                 | 0.6892 | 0.6745 | 0.6172 | 0.6052 | 0.6938 | 0.7101 | 0.6146 | 0.5756 |
| 28     | 0.7072                 | 0.6926 | 0.6719 | 0.6037 | 0.6025 | 0.6740 | 0.5899 | 0.5331 | 0.5116 |
| 29     | 0.6662                 | 0.6270 | 0.6251 | 0.5116 | 0.5061 | 0.5967 | 0.5429 | 0.4975 | 0.5022 |
| 30     | 0.7181                 | 0.6509 | 0.5940 | 0.4886 | 0.4735 | 0.5472 | 0.5069 | 0.4476 | 0.4261 |
| 31     | 0.5960                 | 0.5606 | 0.5187 | 0.4436 | 0.4350 | 0.5461 | 0.5369 | 0.4678 | 0.4622 |



## YEAR 2015 – SMALL HYDRO GENERATION [GW]

| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 32     | 0.6928                | 0.6349 | 0.5858 | 0.4800 | 0.4687 | 0.5463 | 0.5366 | 0.4914 | 0.4742 |
| 33     | 0.6051                | 0.5871 | 0.5285 | 0.4806 | 0.4673 | 0.5544 | 0.5090 | 0.4500 | 0.4258 |
| 34     | 0.6546                | 0.6019 | 0.5374 | 0.4929 | 0.4577 | 0.5761 | 0.5196 | 0.4760 | 0.4512 |
| 35     | 0.6271                | 0.5762 | 0.5329 | 0.4710 | 0.4536 | 0.5002 | 0.4678 | 0.4186 | 0.4049 |
| 36     | 0.6146                | 0.5609 | 0.5078 | 0.4507 | 0.4364 | 0.4813 | 0.4639 | 0.4311 | 0.4198 |
| 37     | 0.5789                | 0.5476 | 0.5075 | 0.4525 | 0.4346 | 0.4940 | 0.4587 | 0.4372 | 0.4159 |
| 38     | 0.5384                | 0.5244 | 0.4944 | 0.4164 | 0.4107 | 0.5805 | 0.5027 | 0.4410 | 0.4229 |
| 39     | 0.5790                | 0.5586 | 0.5239 | 0.4435 | 0.4179 | 0.5153 | 0.4702 | 0.3825 | 0.3724 |
| 40     | 0.4885                | 0.4844 | 0.4544 | 0.3950 | 0.4005 | 0.4220 | 0.3814 | 0.3562 | 0.3518 |
| 41     | 0.4927                | 0.4738 | 0.4551 | 0.3855 | 0.3808 | 0.5560 | 0.4817 | 0.4719 | 0.4198 |
| 42     | 0.6540                | 0.6204 | 0.5732 | 0.5455 | 0.4798 | 0.6582 | 0.6167 | 0.6280 | 0.5798 |
| 43     | 0.5857                | 0.5512 | 0.5138 | 0.4526 | 0.4649 | 0.4443 | 0.4041 | 0.3693 | 0.3410 |
| 44     | 0.4859                | 0.4564 | 0.4213 | 0.3457 | 0.3372 | 0.4105 | 0.3552 | 0.3179 | 0.3119 |
| 45     | 0.6433                | 0.6266 | 0.5814 | 0.5351 | 0.4584 | 0.7399 | 0.7136 | 0.6909 | 0.6955 |
| 46     | 0.7608                | 0.7463 | 0.7254 | 0.6656 | 0.6472 | 0.8143 | 0.7855 | 0.7580 | 0.7698 |
| 47     | 0.8920                | 0.8604 | 0.8468 | 0.8213 | 0.8063 | 0.8417 | 0.8173 | 0.7936 | 0.7589 |
| 48     | 0.8469                | 0.8408 | 0.8114 | 0.7666 | 0.7613 | 0.8977 | 0.8911 | 0.8400 | 0.8690 |
| 49     | 0.9948                | 0.9853 | 0.9612 | 0.9232 | 0.8980 | 0.9642 | 0.8837 | 0.8978 | 0.8886 |
| 50     | 0.9714                | 0.9518 | 0.9181 | 0.8390 | 0.7816 | 0.9996 | 0.9315 | 0.8048 | 0.8209 |
| 51     | 1.0562                | 1.0356 | 1.0027 | 0.9024 | 0.8677 | 0.9352 | 0.8921 | 0.8233 | 0.7469 |
| 52     | 0.9310                | 0.8953 | 0.8413 | 0.7390 | 0.7228 | 0.7349 | 0.6926 | 0.6317 | 0.6238 |

## YEAR 2020 – SMALL HYDRO GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |        |        |        |        |
|--------|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 1      | 1.0664                 | 1.0762 | 1.0573 | 0.9443 | 0.9092 | 1.0651 | 0.9652 | 0.8693 | 0.8706 |
| 2      | 1.1827                 | 1.1335 | 1.1475 | 1.0619 | 1.014  | 1.1452 | 1.0758 | 1.0569 | 0.9511 |
| 3      | 1.1263                 | 1.1403 | 1.1126 | 1.0447 | 1.0402 | 1.1363 | 1.1024 | 1.0874 | 1.0823 |
| 4      | 1.2287                 | 1.2099 | 1.1899 | 1.1362 | 1.1061 | 1.171  | 1.0797 | 1.0358 | 1.0254 |
| 5      | 1.2359                 | 1.2123 | 1.172  | 1.0776 | 1.0133 | 1.1501 | 1.1321 | 1.072  | 1.1096 |
| 6      | 1.2233                 | 1.2097 | 1.1733 | 1.0469 | 1.0266 | 1.0417 | 0.9743 | 0.8836 | 0.8057 |
| 7      | 1.1874                 | 1.1653 | 1.1321 | 0.9817 | 0.8444 | 1.281  | 1.2077 | 1.0006 | 1.0887 |
| 8      | 1.2657                 | 1.2582 | 1.2099 | 1.1524 | 1.0712 | 1.245  | 1.1291 | 1.1405 | 1.115  |
| 9      | 1.295                  | 1.226  | 1.208  | 1.0947 | 1.0513 | 1.1547 | 1.0487 | 1.0054 | 0.8891 |
| 10     | 1.1984                 | 1.1887 | 1.1727 | 1.0331 | 0.9587 | 1.2927 | 1.111  | 1.0412 | 0.8784 |
| 11     | 1.3224                 | 1.2965 | 1.2704 | 1.1276 | 1.1068 | 1.112  | 1.0606 | 1.0524 | 0.9852 |
| 12     | 1.2207                 | 1.1756 | 1.122  | 1.0154 | 0.9928 | 1.0494 | 1.0583 | 0.9236 | 1.0205 |
| 13     | 1.106                  | 1.0773 | 1.0419 | 0.9723 | 0.9625 | 1.0558 | 1.0198 | 0.9854 | 0.9778 |
| 14     | 1.2971                 | 1.2286 | 1.1937 | 1.1289 | 1.0681 | 1.2829 | 1.2259 | 1.1763 | 1.1559 |
| 15     | 1.3121                 | 1.3018 | 1.2777 | 1.2598 | 1.1776 | 1.2757 | 1.1601 | 1.1239 | 1.095  |
| 16     | 1.2587                 | 1.2347 | 1.1933 | 1.1071 | 1.0514 | 1.0685 | 1.0166 | 1.0484 | 0.9768 |
| 17     | 1.0524                 | 1.0292 | 1.0323 | 0.9965 | 0.9633 | 1.1356 | 0.9658 | 0.9618 | 0.8838 |
| 18     | 1.1502                 | 1.0949 | 1.0608 | 1.0401 | 1.0124 | 1.0109 | 0.9787 | 0.9707 | 0.9695 |
| 19     | 0.992                  | 0.9795 | 0.9549 | 0.8829 | 0.8738 | 0.9397 | 0.866  | 0.8243 | 0.8284 |
| 20     | 0.8807                 | 0.8716 | 0.8543 | 0.7977 | 0.7764 | 0.7816 | 0.7682 | 0.76   | 0.7456 |
| 21     | 0.8477                 | 0.8338 | 0.8291 | 0.7368 | 0.7141 | 0.8458 | 0.7989 | 0.8149 | 0.7439 |
| 22     | 0.9652                 | 0.9459 | 0.9016 | 0.8487 | 0.7951 | 0.8437 | 0.8294 | 0.7977 | 0.7623 |
| 23     | 0.8032                 | 0.8346 | 0.8169 | 0.7809 | 0.7506 | 0.8626 | 0.8627 | 0.7685 | 0.8633 |
| 24     | 0.9268                 | 0.8905 | 0.8491 | 0.771  | 0.7441 | 0.7668 | 0.7392 | 0.7005 | 0.6794 |
| 25     | 0.8869                 | 0.8152 | 0.7402 | 0.6494 | 0.6415 | 0.7276 | 0.7185 | 0.6242 | 0.631  |
| 26     | 0.9052                 | 0.859  | 0.8051 | 0.7445 | 0.6945 | 0.7653 | 0.7462 | 0.7168 | 0.6846 |
| 27     | 0.8122                 | 0.753  | 0.737  | 0.6744 | 0.6613 | 0.7581 | 0.7759 | 0.6715 | 0.6289 |
| 28     | 0.7727                 | 0.7568 | 0.7341 | 0.6596 | 0.6583 | 0.7364 | 0.6445 | 0.5825 | 0.559  |
| 29     | 0.7279                 | 0.6851 | 0.683  | 0.559  | 0.553  | 0.652  | 0.5932 | 0.5436 | 0.5487 |
| 30     | 0.7846                 | 0.7112 | 0.649  | 0.5339 | 0.5174 | 0.5979 | 0.5539 | 0.4891 | 0.4656 |
| 31     | 0.6512                 | 0.6125 | 0.5668 | 0.4847 | 0.4753 | 0.5967 | 0.5866 | 0.5111 | 0.505  |

## YEAR 2020 – SMALL HYDRO GENERATION [GW]

| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 32     | 0.757                 | 0.6937 | 0.6401 | 0.5245 | 0.5121 | 0.5969 | 0.5863 | 0.5369 | 0.5181 |
| 33     | 0.6612                | 0.6415 | 0.5775 | 0.5251 | 0.5106 | 0.6058 | 0.5562 | 0.4917 | 0.4652 |
| 34     | 0.7152                | 0.6577 | 0.5872 | 0.5386 | 0.5001 | 0.6295 | 0.5677 | 0.5201 | 0.493  |
| 35     | 0.6852                | 0.6296 | 0.5823 | 0.5146 | 0.4956 | 0.5465 | 0.5111 | 0.4574 | 0.4424 |
| 36     | 0.6715                | 0.6129 | 0.5548 | 0.4925 | 0.4768 | 0.5259 | 0.5069 | 0.471  | 0.4587 |
| 37     | 0.6325                | 0.5983 | 0.5545 | 0.4944 | 0.4749 | 0.5398 | 0.5012 | 0.4777 | 0.4544 |
| 38     | 0.5883                | 0.573  | 0.5402 | 0.455  | 0.4487 | 0.6343 | 0.5493 | 0.4819 | 0.4621 |
| 39     | 0.6326                | 0.6103 | 0.5724 | 0.4846 | 0.4566 | 0.563  | 0.5138 | 0.4179 | 0.4069 |
| 40     | 0.5338                | 0.5293 | 0.4965 | 0.4316 | 0.4376 | 0.4611 | 0.4167 | 0.3892 | 0.3844 |
| 41     | 0.5383                | 0.5177 | 0.4973 | 0.4212 | 0.4161 | 0.6075 | 0.5263 | 0.5156 | 0.4587 |
| 42     | 0.7146                | 0.6779 | 0.6263 | 0.596  | 0.5242 | 0.7192 | 0.6738 | 0.6862 | 0.6335 |
| 43     | 0.64                  | 0.6023 | 0.5614 | 0.4945 | 0.508  | 0.4855 | 0.4415 | 0.4035 | 0.3726 |
| 44     | 0.5309                | 0.4987 | 0.4603 | 0.3777 | 0.3684 | 0.4485 | 0.3881 | 0.3473 | 0.3408 |
| 45     | 0.7029                | 0.6846 | 0.6353 | 0.5847 | 0.5009 | 0.8084 | 0.7797 | 0.7549 | 0.7599 |
| 46     | 0.8313                | 0.8154 | 0.7926 | 0.7273 | 0.7072 | 0.8897 | 0.8583 | 0.8282 | 0.8411 |
| 47     | 0.9746                | 0.9401 | 0.9252 | 0.8974 | 0.881  | 0.9197 | 0.893  | 0.8671 | 0.8292 |
| 48     | 0.9254                | 0.9187 | 0.8866 | 0.8376 | 0.8318 | 0.9809 | 0.9736 | 0.9178 | 0.9495 |
| 49     | 1.087                 | 1.0766 | 1.0502 | 1.0087 | 0.9812 | 1.0535 | 0.9656 | 0.981  | 0.9709 |
| 50     | 1.0614                | 1.04   | 1.0031 | 0.9167 | 0.854  | 1.0922 | 1.0178 | 0.8794 | 0.8969 |
| 51     | 1.154                 | 1.1315 | 1.0956 | 0.986  | 0.9481 | 1.0218 | 0.9747 | 0.8996 | 0.8161 |
| 52     | 1.0172                | 0.9782 | 0.9192 | 0.8075 | 0.7898 | 0.803  | 0.7568 | 0.6902 | 0.6816 |

## YEAR 2015 – NON-RENEWABLE THERMAL GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |        |        |        |        |
|--------|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 1      | 3.6692                 | 3.6035 | 3.2561 | 2.5220 | 2.3077 | 2.5130 | 2.3066 | 2.2009 | 2.0789 |
| 2      | 3.9541                 | 3.8924 | 3.8079 | 2.9721 | 2.7759 | 2.8745 | 2.8915 | 2.8218 | 2.5067 |
| 3      | 3.9023                 | 3.8697 | 3.7703 | 2.8883 | 2.8386 | 2.8390 | 2.7931 | 2.8364 | 2.8192 |
| 4      | 3.9252                 | 3.8691 | 3.7786 | 2.9834 | 2.9148 | 2.7467 | 2.6623 | 2.7264 | 2.7590 |
| 5      | 3.7716                 | 3.7204 | 3.6088 | 2.7431 | 2.6665 | 2.6092 | 2.5923 | 2.4718 | 2.6026 |
| 6      | 3.6544                 | 3.5824 | 3.3806 | 2.6013 | 2.5319 | 2.1932 | 2.1076 | 2.0374 | 1.9420 |
| 7      | 3.0765                 | 2.9770 | 2.7026 | 2.1347 | 1.9278 | 2.0613 | 1.9718 | 1.8399 | 1.8271 |
| 8      | 2.9183                 | 2.8643 | 2.7272 | 2.1567 | 2.0100 | 1.9568 | 1.8962 | 1.9540 | 1.9704 |
| 9      | 2.7824                 | 2.5859 | 2.5494 | 2.0239 | 1.9614 | 1.7605 | 1.6635 | 1.6188 | 1.5401 |
| 10     | 2.1708                 | 2.4804 | 2.4448 | 1.8512 | 1.7417 | 1.6400 | 1.5601 | 1.5515 | 1.3796 |
| 11     | 2.9226                 | 2.8320 | 2.7756 | 2.1580 | 2.0236 | 1.9426 | 1.8511 | 1.8741 | 1.6947 |
| 12     | 2.8984                 | 2.8174 | 2.7462 | 2.2211 | 2.1273 | 1.7095 | 1.6674 | 1.6925 | 1.4873 |
| 13     | 2.4590                 | 2.5184 | 2.4741 | 1.9880 | 1.9194 | 1.8782 | 1.8706 | 1.8709 | 1.8499 |
| 14     | 2.4634                 | 2.4765 | 2.3640 | 1.9636 | 1.8792 | 1.7160 | 1.6537 | 1.6285 | 1.6868 |
| 15     | 2.5298                 | 2.5382 | 2.4619 | 2.0180 | 1.9264 | 1.5725 | 1.5200 | 1.5184 | 1.4866 |
| 16     | 2.3630                 | 2.3828 | 2.2849 | 1.8561 | 1.7340 | 1.7137 | 1.6258 | 1.5995 | 1.5166 |
| 17     | 2.2805                 | 2.2760 | 2.1517 | 1.8974 | 1.7314 | 1.5388 | 1.4856 | 1.4549 | 1.3424 |
| 18     | 2.6087                 | 2.5632 | 2.2029 | 1.9281 | 1.7479 | 1.6839 | 1.6962 | 1.6549 | 1.6297 |
| 19     | 2.6736                 | 2.6805 | 2.6064 | 2.1214 | 1.9742 | 2.0175 | 2.0350 | 2.0561 | 2.0098 |
| 20     | 2.7702                 | 2.7837 | 2.7153 | 2.1522 | 2.0915 | 1.9924 | 2.0239 | 1.9696 | 2.0339 |
| 21     | 2.7437                 | 2.7429 | 2.7209 | 2.1537 | 2.0841 | 2.2988 | 2.2010 | 2.2014 | 2.1402 |
| 22     | 2.8832                 | 2.9058 | 2.8485 | 2.3824 | 2.2655 | 2.2838 | 2.2627 | 2.2620 | 2.1916 |
| 23     | 2.7930                 | 2.9491 | 2.9284 | 2.4971 | 2.3554 | 2.3332 | 2.2885 | 2.3825 | 2.3184 |
| 24     | 3.0143                 | 3.0013 | 2.9507 | 2.5998 | 2.4993 | 2.3403 | 2.1924 | 2.2888 | 2.0929 |
| 25     | 2.9633                 | 2.9650 | 2.9186 | 2.5736 | 2.4425 | 2.3792 | 2.3753 | 2.3993 | 2.3298 |
| 26     | 2.8779                 | 2.8776 | 2.8483 | 2.5568 | 2.4781 | 2.2808 | 2.2806 | 2.3458 | 2.1376 |
| 27     | 2.8393                 | 2.8430 | 2.8177 | 2.4824 | 2.3944 | 2.2982 | 2.2886 | 2.3398 | 2.0781 |
| 28     | 2.8699                 | 2.8636 | 2.8068 | 2.4387 | 2.2989 | 2.4696 | 2.4049 | 2.3858 | 2.3371 |
| 29     | 2.9983                 | 2.9881 | 2.9673 | 2.7158 | 2.5941 | 2.3686 | 2.2562 | 2.3796 | 2.2060 |
| 30     | 2.8891                 | 2.8735 | 2.8078 | 2.5324 | 2.4636 | 2.2663 | 2.2237 | 2.2834 | 2.1963 |
| 31     | 2.7070                 | 2.6674 | 2.6430 | 2.3840 | 2.3328 | 2.3298 | 2.1987 | 2.3352 | 2.1610 |

## YEAR 2015 – NON-RENEWABLE THERMAL GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |        |        |        |        |
|--------|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
|        | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 32     | 2.5742                 | 2.5721 | 2.5393 | 2.3467 | 2.2737 | 2.3296 | 2.2752 | 2.3350 | 2.2569 |
| 33     | 2.5721                 | 2.5542 | 2.3894 | 2.2974 | 2.2682 | 2.2154 | 2.2007 | 2.2173 | 2.1748 |
| 34     | 2.6999                 | 2.6822 | 2.6499 | 2.4648 | 2.3806 | 2.3340 | 2.2944 | 2.3437 | 2.2749 |
| 35     | 2.6731                 | 2.6784 | 2.6565 | 2.4617 | 2.3721 | 2.3098 | 2.2917 | 2.2823 | 2.2699 |
| 36     | 2.8308                 | 2.8358 | 2.8185 | 2.5663 | 2.5115 | 2.4997 | 2.4212 | 2.5165 | 2.3590 |
| 37     | 2.8697                 | 2.8418 | 2.8117 | 2.5820 | 2.5381 | 2.4857 | 2.4347 | 2.4698 | 2.4008 |
| 38     | 2.8524                 | 2.8548 | 2.8354 | 2.5519 | 2.4717 | 2.5765 | 2.5113 | 2.5662 | 2.4424 |
| 39     | 2.9303                 | 2.9186 | 2.8856 | 2.6163 | 2.5698 | 2.5073 | 2.4729 | 2.5113 | 2.3887 |
| 40     | 2.9599                 | 2.9684 | 2.9182 | 2.6710 | 2.5912 | 2.6047 | 2.5163 | 2.5364 | 2.3578 |
| 41     | 2.9341                 | 2.9401 | 2.9050 | 2.5061 | 2.4432 | 2.5446 | 2.3617 | 2.5077 | 2.0167 |
| 42     | 2.9703                 | 2.9305 | 2.7564 | 2.3336 | 2.1905 | 2.4440 | 2.3210 | 2.3414 | 2.1850 |
| 43     | 3.0054                 | 2.9872 | 2.9529 | 2.5683 | 2.4436 | 2.5967 | 2.5372 | 2.4835 | 2.3611 |
| 44     | 2.9624                 | 2.9447 | 2.8989 | 2.5611 | 2.4820 | 2.4370 | 2.3520 | 2.4352 | 2.1498 |
| 45     | 2.9208                 | 2.8741 | 2.8010 | 2.3651 | 2.2418 | 2.4106 | 2.3727 | 2.3683 | 2.2204 |
| 46     | 2.8746                 | 2.8597 | 2.7741 | 2.3075 | 2.2240 | 2.0056 | 1.8864 | 1.9387 | 1.6885 |
| 47     | 2.7962                 | 2.7808 | 2.7205 | 2.3106 | 2.1878 | 2.3087 | 2.1669 | 2.2631 | 1.7880 |
| 48     | 2.8912                 | 2.8523 | 2.7968 | 2.3868 | 2.2570 | 2.3088 | 2.1152 | 2.1952 | 1.8452 |
| 49     | 2.8707                 | 2.7845 | 2.6193 | 2.2697 | 2.0933 | 2.3046 | 2.2175 | 2.1256 | 2.0012 |
| 50     | 2.9138                 | 2.8692 | 2.8211 | 2.4408 | 2.3088 | 2.4624 | 2.3953 | 2.3145 | 2.2464 |
| 51     | 2.9090                 | 2.8748 | 2.8415 | 2.4701 | 2.4037 | 2.5413 | 2.4846 | 2.4092 | 2.3084 |
| 52     | 2.7900                 | 2.6320 | 2.1691 | 2.0888 | 1.9004 | 1.8223 | 1.6213 | 1.5009 | 1.4205 |

## YEAR 2020 – NON-RENEWABLE THERMAL GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |        |        |        |        |
|--------|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 1      | 4.5556                 | 4.474  | 4.0427 | 3.1313 | 2.8652 | 3.1201 | 2.8638 | 2.7326 | 2.5811 |
| 2      | 4.9093                 | 4.8327 | 4.7278 | 3.6901 | 3.4465 | 3.5689 | 3.59   | 3.5035 | 3.1123 |
| 3      | 4.845                  | 4.8046 | 4.6811 | 3.5861 | 3.5244 | 3.5249 | 3.4679 | 3.5216 | 3.5003 |
| 4      | 4.8735                 | 4.8038 | 4.6914 | 3.7041 | 3.619  | 3.4103 | 3.3055 | 3.3851 | 3.4255 |
| 5      | 4.6828                 | 4.6192 | 4.4806 | 3.4058 | 3.3107 | 3.2395 | 3.2186 | 3.0689 | 3.2313 |
| 6      | 4.5372                 | 4.4479 | 4.1973 | 3.2297 | 3.1436 | 2.723  | 2.6168 | 2.5296 | 2.4112 |
| 7      | 3.8197                 | 3.6962 | 3.3555 | 2.6504 | 2.3935 | 2.5593 | 2.4482 | 2.2844 | 2.2685 |
| 8      | 3.6233                 | 3.5563 | 3.386  | 2.6777 | 2.4956 | 2.4295 | 2.3543 | 2.4261 | 2.4464 |
| 9      | 3.4546                 | 3.2106 | 3.1653 | 2.5128 | 2.4352 | 2.1858 | 2.0654 | 2.0099 | 1.9122 |
| 10     | 2.6952                 | 3.0796 | 3.0354 | 2.2984 | 2.1625 | 2.0362 | 1.937  | 1.9263 | 1.7129 |
| 11     | 3.6287                 | 3.5162 | 3.4461 | 2.6793 | 2.5125 | 2.4119 | 2.2983 | 2.3269 | 2.1041 |
| 12     | 3.5986                 | 3.498  | 3.4096 | 2.7577 | 2.6412 | 2.1225 | 2.0702 | 2.1014 | 1.8466 |
| 13     | 3.0531                 | 3.1268 | 3.0718 | 2.4683 | 2.3831 | 2.3319 | 2.3225 | 2.3229 | 2.2968 |
| 14     | 3.0585                 | 3.0748 | 2.9351 | 2.438  | 2.3332 | 2.1306 | 2.0532 | 2.0219 | 2.0943 |
| 15     | 3.141                  | 3.1514 | 3.0567 | 2.5055 | 2.3918 | 1.9524 | 1.8872 | 1.8852 | 1.8457 |
| 16     | 2.9339                 | 2.9584 | 2.8369 | 2.3045 | 2.1529 | 2.1277 | 2.0186 | 1.9859 | 1.883  |
| 17     | 2.8314                 | 2.8258 | 2.6715 | 2.3558 | 2.1497 | 1.9105 | 1.8445 | 1.8064 | 1.6667 |
| 18     | 3.2389                 | 3.1824 | 2.7351 | 2.3939 | 2.1702 | 2.0907 | 2.106  | 2.0547 | 2.0234 |
| 19     | 3.3195                 | 3.3281 | 3.2361 | 2.6339 | 2.4511 | 2.5049 | 2.5266 | 2.5528 | 2.4953 |
| 20     | 3.4394                 | 3.4562 | 3.3713 | 2.6721 | 2.5968 | 2.4737 | 2.5128 | 2.4454 | 2.5253 |
| 21     | 3.4065                 | 3.4055 | 3.3782 | 2.674  | 2.5876 | 2.8542 | 2.7327 | 2.7332 | 2.6572 |
| 22     | 3.5797                 | 3.6078 | 3.5367 | 2.958  | 2.8128 | 2.8355 | 2.8093 | 2.8085 | 2.7211 |
| 23     | 3.4677                 | 3.6616 | 3.6359 | 3.1004 | 2.9244 | 2.8969 | 2.8414 | 2.9581 | 2.8785 |
| 24     | 3.7425                 | 3.7264 | 3.6635 | 3.2279 | 3.1031 | 2.9057 | 2.722  | 2.8417 | 2.5985 |
| 25     | 3.6792                 | 3.6813 | 3.6237 | 3.1953 | 3.0326 | 2.954  | 2.9491 | 2.9789 | 2.8926 |
| 26     | 3.5732                 | 3.5728 | 3.5364 | 3.1745 | 3.0768 | 2.8318 | 2.8316 | 2.9125 | 2.654  |
| 27     | 3.5252                 | 3.5298 | 3.4984 | 3.0821 | 2.9728 | 2.8534 | 2.8415 | 2.9051 | 2.5801 |
| 28     | 3.5632                 | 3.5554 | 3.4849 | 3.0279 | 2.8543 | 3.0662 | 2.9859 | 2.9622 | 2.9017 |
| 29     | 3.7226                 | 3.71   | 3.6842 | 3.3719 | 3.2208 | 2.9408 | 2.8013 | 2.9545 | 2.7389 |
| 30     | 3.5871                 | 3.5677 | 3.4861 | 3.1442 | 3.0588 | 2.8138 | 2.7609 | 2.835  | 2.7269 |
| 31     | 3.361                  | 3.3118 | 3.2815 | 2.9599 | 2.8964 | 2.8926 | 2.7299 | 2.8993 | 2.6831 |

## YEAR 2020 – NON-RENEWABLE THERMAL GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |        |        |        |        |
|--------|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 32     | 3.1961                 | 3.1935 | 3.1528 | 2.9136 | 2.823  | 2.8924 | 2.8249 | 2.8991 | 2.8021 |
| 33     | 3.1935                 | 3.1713 | 2.9666 | 2.8524 | 2.8162 | 2.7506 | 2.7324 | 2.753  | 2.7002 |
| 34     | 3.3522                 | 3.3302 | 3.2901 | 3.0603 | 2.9557 | 2.8979 | 2.8487 | 2.9099 | 2.8245 |
| 35     | 3.3189                 | 3.3255 | 3.2983 | 3.0564 | 2.9452 | 2.8678 | 2.8453 | 2.8337 | 2.8183 |
| 36     | 3.5147                 | 3.5209 | 3.4994 | 3.1863 | 3.1182 | 3.1036 | 3.0061 | 3.1244 | 2.9289 |
| 37     | 3.563                  | 3.5283 | 3.491  | 3.2058 | 3.1513 | 3.0862 | 3.0229 | 3.0665 | 2.9808 |
| 38     | 3.5415                 | 3.5445 | 3.5204 | 3.1684 | 3.0688 | 3.1989 | 3.118  | 3.1862 | 3.0324 |
| 39     | 3.6382                 | 3.6237 | 3.5827 | 3.2484 | 3.1906 | 3.113  | 3.0703 | 3.118  | 2.9658 |
| 40     | 3.675                  | 3.6855 | 3.6232 | 3.3163 | 3.2172 | 3.234  | 3.1242 | 3.1492 | 2.9274 |
| 41     | 3.6429                 | 3.6504 | 3.6068 | 3.1115 | 3.0334 | 3.1593 | 2.9322 | 3.1135 | 2.5039 |
| 42     | 3.6879                 | 3.6385 | 3.4223 | 2.8974 | 2.7197 | 3.0344 | 2.8817 | 2.907  | 2.7129 |
| 43     | 3.7315                 | 3.7089 | 3.6663 | 3.1888 | 3.0339 | 3.224  | 3.1501 | 3.0835 | 2.9315 |
| 44     | 3.6781                 | 3.6561 | 3.5992 | 3.1798 | 3.0816 | 3.0257 | 2.9202 | 3.0235 | 2.6692 |
| 45     | 3.6264                 | 3.5684 | 3.4777 | 2.9365 | 2.7834 | 2.993  | 2.9459 | 2.9404 | 2.7568 |
| 46     | 3.5691                 | 3.5506 | 3.4443 | 2.865  | 2.7613 | 2.4901 | 2.3421 | 2.4071 | 2.0964 |
| 47     | 3.4717                 | 3.4526 | 3.3777 | 2.8688 | 2.7163 | 2.8664 | 2.6904 | 2.8098 | 2.22   |
| 48     | 3.5897                 | 3.5414 | 3.4725 | 2.9634 | 2.8023 | 2.8666 | 2.6262 | 2.7255 | 2.291  |
| 49     | 3.5642                 | 3.4572 | 3.2521 | 2.818  | 2.599  | 2.8614 | 2.7532 | 2.6391 | 2.4847 |
| 50     | 3.6177                 | 3.5624 | 3.5026 | 3.0305 | 2.8666 | 3.0573 | 2.974  | 2.8736 | 2.7891 |
| 51     | 3.6118                 | 3.5693 | 3.528  | 3.0668 | 2.9844 | 3.1552 | 3.0848 | 2.9912 | 2.8661 |
| 52     | 3.464                  | 3.2678 | 2.6931 | 2.5934 | 2.3595 | 2.2625 | 2.013  | 1.8635 | 1.7637 |

## YEAR 2015 – RENEWABLE THERMAL GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |        |        |        |        |
|--------|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 1      | 0.5917                 | 0.5915 | 0.5785 | 0.5563 | 0.5153 | 0.5672 | 0.5451 | 0.4776 | 0.4909 |
| 2      | 0.5973                 | 0.5763 | 0.5844 | 0.5576 | 0.5227 | 0.6056 | 0.5856 | 0.5940 | 0.5553 |
| 3      | 0.6126                 | 0.6114 | 0.6106 | 0.5912 | 0.5868 | 0.5623 | 0.5506 | 0.5950 | 0.5641 |
| 4      | 0.5614                 | 0.5637 | 0.5627 | 0.5332 | 0.5304 | 0.6067 | 0.5866 | 0.5965 | 0.6082 |
| 5      | 0.6034                 | 0.5853 | 0.5882 | 0.5639 | 0.5340 | 0.5566 | 0.5109 | 0.4794 | 0.4916 |
| 6      | 0.5753                 | 0.5586 | 0.5340 | 0.4953 | 0.4734 | 0.4265 | 0.3978 | 0.3553 | 0.3190 |
| 7      | 0.4601                 | 0.4641 | 0.4299 | 0.3667 | 0.3047 | 0.4814 | 0.4478 | 0.3499 | 0.3695 |
| 8      | 0.4896                 | 0.4929 | 0.4796 | 0.4419 | 0.3927 | 0.5075 | 0.4520 | 0.4852 | 0.4560 |
| 9      | 0.5336                 | 0.4971 | 0.5049 | 0.4565 | 0.4228 | 0.4172 | 0.3700 | 0.3912 | 0.3301 |
| 10     | 0.4398                 | 0.4465 | 0.4440 | 0.3921 | 0.3649 | 0.4829 | 0.4283 | 0.4202 | 0.3583 |
| 11     | 0.5255                 | 0.5193 | 0.5250 | 0.4964 | 0.4706 | 0.5356 | 0.5171 | 0.5177 | 0.4863 |
| 12     | 0.5578                 | 0.5515 | 0.5485 | 0.5172 | 0.5019 | 0.4769 | 0.4707 | 0.4698 | 0.4505 |
| 13     | 0.4579                 | 0.4634 | 0.4666 | 0.4399 | 0.4215 | 0.4574 | 0.4481 | 0.4542 | 0.4457 |
| 14     | 0.4706                 | 0.4631 | 0.4650 | 0.4505 | 0.4311 | 0.4649 | 0.4575 | 0.4609 | 0.4556 |
| 15     | 0.4785                 | 0.4709 | 0.4737 | 0.4549 | 0.4443 | 0.4506 | 0.4533 | 0.4447 | 0.4294 |
| 16     | 0.4843                 | 0.4816 | 0.4790 | 0.4587 | 0.4415 | 0.4695 | 0.4700 | 0.4577 | 0.4634 |
| 17     | 0.4984                 | 0.4844 | 0.4664 | 0.4682 | 0.4455 | 0.4714 | 0.4461 | 0.4605 | 0.4310 |
| 18     | 0.5361                 | 0.5270 | 0.5204 | 0.5078 | 0.4976 | 0.4947 | 0.4903 | 0.5003 | 0.5006 |
| 19     | 0.5017                 | 0.5036 | 0.5004 | 0.4843 | 0.4803 | 0.5399 | 0.5426 | 0.5282 | 0.5425 |
| 20     | 0.5616                 | 0.5642 | 0.5698 | 0.5546 | 0.5516 | 0.5621 | 0.5722 | 0.5493 | 0.5726 |
| 21     | 0.5825                 | 0.5791 | 0.5783 | 0.5510 | 0.5535 | 0.5809 | 0.5765 | 0.5815 | 0.5813 |
| 22     | 0.6083                 | 0.6171 | 0.6135 | 0.6013 | 0.5882 | 0.5896 | 0.5827 | 0.5840 | 0.5922 |
| 23     | 0.6182                 | 0.6140 | 0.6120 | 0.6067 | 0.5936 | 0.6196 | 0.6176 | 0.6095 | 0.6242 |
| 24     | 0.6447                 | 0.6438 | 0.6421 | 0.6255 | 0.6205 | 0.6136 | 0.6000 | 0.6059 | 0.5923 |
| 25     | 0.6116                 | 0.6080 | 0.5975 | 0.5926 | 0.5915 | 0.5610 | 0.5524 | 0.5606 | 0.5452 |
| 26     | 0.5156                 | 0.5033 | 0.4885 | 0.4934 | 0.4885 | 0.5117 | 0.5164 | 0.5584 | 0.4936 |
| 27     | 0.5631                 | 0.5455 | 0.5606 | 0.5383 | 0.5305 | 0.5989 | 0.5931 | 0.5978 | 0.5762 |
| 28     | 0.6043                 | 0.6127 | 0.6046 | 0.5908 | 0.5913 | 0.5562 | 0.5348 | 0.5449 | 0.5148 |
| 29     | 0.5564                 | 0.5609 | 0.5603 | 0.5485 | 0.5469 | 0.5345 | 0.5506 | 0.5439 | 0.5570 |
| 30     | 0.5610                 | 0.5473 | 0.5550 | 0.5441 | 0.5487 | 0.5397 | 0.5614 | 0.5477 | 0.5579 |
| 31     | 0.5936                 | 0.5959 | 0.5997 | 0.5878 | 0.5855 | 0.5908 | 0.5849 | 0.5844 | 0.5612 |



## YEAR 2015 - RENEWABLE THERMAL GENERATION [GW]

| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 32     | 0.6074                | 0.6129 | 0.6058 | 0.5957 | 0.5926 | 0.6079 | 0.5993 | 0.6034 | 0.6014 |
| 33     | 0.6083                | 0.6036 | 0.5943 | 0.5960 | 0.5923 | 0.5827 | 0.5818 | 0.5831 | 0.5788 |
| 34     | 0.6013                | 0.6013 | 0.5970 | 0.5930 | 0.5881 | 0.5851 | 0.5869 | 0.5846 | 0.5826 |
| 35     | 0.5864                | 0.5863 | 0.5752 | 0.5746 | 0.5701 | 0.6047 | 0.6032 | 0.6010 | 0.5944 |
| 36     | 0.6105                | 0.6073 | 0.6043 | 0.5999 | 0.5988 | 0.5851 | 0.5868 | 0.5989 | 0.5814 |
| 37     | 0.5498                | 0.5550 | 0.5471 | 0.5327 | 0.5370 | 0.5901 | 0.5829 | 0.5821 | 0.5823 |
| 38     | 0.5682                | 0.5733 | 0.5727 | 0.5658 | 0.5636 | 0.5835 | 0.5905 | 0.5754 | 0.5899 |
| 39     | 0.6161                | 0.6232 | 0.6259 | 0.5987 | 0.5972 | 0.6246 | 0.6194 | 0.6130 | 0.6073 |
| 40     | 0.5673                | 0.5796 | 0.5718 | 0.5505 | 0.5575 | 0.5836 | 0.5732 | 0.5697 | 0.5709 |
| 41     | 0.5665                | 0.5704 | 0.5588 | 0.5467 | 0.5464 | 0.4544 | 0.4262 | 0.4633 | 0.4063 |
| 42     | 0.4951                | 0.4870 | 0.4526 | 0.4437 | 0.4093 | 0.4977 | 0.4915 | 0.4906 | 0.4877 |
| 43     | 0.5150                | 0.5183 | 0.5218 | 0.4893 | 0.4823 | 0.5296 | 0.5175 | 0.5239 | 0.4963 |
| 44     | 0.5568                | 0.5503 | 0.5479 | 0.5189 | 0.5223 | 0.5409 | 0.5357 | 0.5294 | 0.5323 |
| 45     | 0.5530                | 0.5459 | 0.5412 | 0.5244 | 0.5227 | 0.5112 | 0.5134 | 0.5123 | 0.5190 |
| 46     | 0.5226                | 0.5179 | 0.5132 | 0.4910 | 0.4832 | 0.5220 | 0.5157 | 0.5132 | 0.5128 |
| 47     | 0.5324                | 0.5148 | 0.5106 | 0.4951 | 0.4891 | 0.5036 | 0.4928 | 0.4884 | 0.4595 |
| 48     | 0.5438                | 0.5394 | 0.5327 | 0.5201 | 0.5144 | 0.5345 | 0.5239 | 0.5266 | 0.5181 |
| 49     | 0.5536                | 0.5455 | 0.5345 | 0.5043 | 0.4900 | 0.5840 | 0.5730 | 0.5534 | 0.5494 |
| 50     | 0.5785                | 0.5714 | 0.5694 | 0.5566 | 0.5519 | 0.5826 | 0.5778 | 0.5523 | 0.5706 |
| 51     | 0.5932                | 0.5825 | 0.5801 | 0.5598 | 0.5541 | 0.5782 | 0.5688 | 0.5596 | 0.5527 |
| 52     | 0.5060                | 0.5136 | 0.5135 | 0.5003 | 0.4862 | 0.5120 | 0.5029 | 0.4834 | 0.4652 |

## YEAR 2020 – RENEWABLE THERMAL GENERATION [GW]

| Period | Sub-period /Load level |        |        |        |        |        |        |        |        |
|--------|------------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                 | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 1      | 0.618                  | 0.6178 | 0.6043 | 0.5811 | 0.5382 | 0.5925 | 0.5694 | 0.4989 | 0.5128 |
| 2      | 0.6239                 | 0.602  | 0.6104 | 0.5824 | 0.546  | 0.6326 | 0.6117 | 0.6204 | 0.58   |
| 3      | 0.6399                 | 0.6386 | 0.6378 | 0.6175 | 0.6129 | 0.5873 | 0.5751 | 0.6215 | 0.5892 |
| 4      | 0.5864                 | 0.5888 | 0.5878 | 0.5569 | 0.554  | 0.6337 | 0.6127 | 0.6231 | 0.6353 |
| 5      | 0.6303                 | 0.6114 | 0.6144 | 0.589  | 0.5578 | 0.5814 | 0.5336 | 0.5007 | 0.5135 |
| 6      | 0.6009                 | 0.5835 | 0.5578 | 0.5174 | 0.4945 | 0.4455 | 0.4155 | 0.3711 | 0.3332 |
| 7      | 0.4806                 | 0.4848 | 0.449  | 0.383  | 0.3183 | 0.5028 | 0.4677 | 0.3655 | 0.386  |
| 8      | 0.5114                 | 0.5148 | 0.501  | 0.4616 | 0.4102 | 0.5301 | 0.4721 | 0.5068 | 0.4763 |
| 9      | 0.5574                 | 0.5192 | 0.5274 | 0.4768 | 0.4416 | 0.4358 | 0.3865 | 0.4086 | 0.3448 |
| 10     | 0.4594                 | 0.4664 | 0.4638 | 0.4096 | 0.3811 | 0.5044 | 0.4474 | 0.4389 | 0.3743 |
| 11     | 0.5489                 | 0.5424 | 0.5484 | 0.5185 | 0.4916 | 0.5594 | 0.5401 | 0.5407 | 0.508  |
| 12     | 0.5826                 | 0.5761 | 0.5729 | 0.5402 | 0.5242 | 0.4981 | 0.4917 | 0.4907 | 0.4706 |
| 13     | 0.4783                 | 0.484  | 0.4874 | 0.4595 | 0.4403 | 0.4778 | 0.4681 | 0.4744 | 0.4655 |
| 14     | 0.4916                 | 0.4837 | 0.4857 | 0.4706 | 0.4503 | 0.4856 | 0.4779 | 0.4814 | 0.4759 |
| 15     | 0.4998                 | 0.4919 | 0.4948 | 0.4752 | 0.4641 | 0.4707 | 0.4735 | 0.4645 | 0.4485 |
| 16     | 0.5059                 | 0.503  | 0.5003 | 0.4791 | 0.4612 | 0.4904 | 0.4909 | 0.4781 | 0.484  |
| 17     | 0.5206                 | 0.506  | 0.4872 | 0.489  | 0.4653 | 0.4924 | 0.466  | 0.481  | 0.4502 |
| 18     | 0.56                   | 0.5505 | 0.5436 | 0.5304 | 0.5198 | 0.5167 | 0.5121 | 0.5226 | 0.5229 |
| 19     | 0.524                  | 0.526  | 0.5227 | 0.5059 | 0.5017 | 0.5639 | 0.5668 | 0.5517 | 0.5667 |
| 20     | 0.5866                 | 0.5893 | 0.5952 | 0.5793 | 0.5762 | 0.5871 | 0.5977 | 0.5738 | 0.5981 |
| 21     | 0.6084                 | 0.6049 | 0.604  | 0.5755 | 0.5781 | 0.6068 | 0.6022 | 0.6074 | 0.6072 |
| 22     | 0.6354                 | 0.6446 | 0.6408 | 0.6281 | 0.6144 | 0.6159 | 0.6086 | 0.61   | 0.6186 |
| 23     | 0.6457                 | 0.6413 | 0.6392 | 0.6337 | 0.62   | 0.6472 | 0.6451 | 0.6366 | 0.652  |
| 24     | 0.6734                 | 0.6725 | 0.6707 | 0.6533 | 0.6481 | 0.6409 | 0.6267 | 0.6329 | 0.6187 |
| 25     | 0.6388                 | 0.6351 | 0.6241 | 0.619  | 0.6178 | 0.586  | 0.577  | 0.5856 | 0.5695 |
| 26     | 0.5386                 | 0.5257 | 0.5102 | 0.5154 | 0.5102 | 0.5345 | 0.5394 | 0.5833 | 0.5156 |
| 27     | 0.5882                 | 0.5698 | 0.5856 | 0.5623 | 0.5541 | 0.6256 | 0.6195 | 0.6244 | 0.6019 |
| 28     | 0.6312                 | 0.64   | 0.6315 | 0.6171 | 0.6176 | 0.581  | 0.5586 | 0.5692 | 0.5377 |
| 29     | 0.5812                 | 0.5859 | 0.5852 | 0.5729 | 0.5712 | 0.5583 | 0.5751 | 0.5681 | 0.5818 |
| 30     | 0.586                  | 0.5717 | 0.5797 | 0.5683 | 0.5731 | 0.5637 | 0.5864 | 0.5721 | 0.5827 |
| 31     | 0.62                   | 0.6224 | 0.6264 | 0.614  | 0.6116 | 0.6171 | 0.6109 | 0.6104 | 0.5862 |

## YEAR 2020 - RENEWABLE THERMAL GENERATION [GW]

| Period | Sub-period/Load level |        |        |        |        |        |        |        |        |
|--------|-----------------------|--------|--------|--------|--------|--------|--------|--------|--------|
| Week   | lab.n1                | lab.n2 | lab.n3 | lab.n4 | lab.n5 | fes.n1 | fes.n2 | fes.n3 | fes.n4 |
| 32     | 0.6344                | 0.6402 | 0.6328 | 0.6222 | 0.619  | 0.635  | 0.626  | 0.6303 | 0.6282 |
| 33     | 0.6354                | 0.6305 | 0.6208 | 0.6225 | 0.6187 | 0.6086 | 0.6077 | 0.6091 | 0.6046 |
| 34     | 0.6281                | 0.6281 | 0.6236 | 0.6194 | 0.6143 | 0.6112 | 0.613  | 0.6106 | 0.6085 |
| 35     | 0.6125                | 0.6124 | 0.6008 | 0.6002 | 0.5955 | 0.6316 | 0.6301 | 0.6278 | 0.6209 |
| 36     | 0.6377                | 0.6343 | 0.6312 | 0.6266 | 0.6255 | 0.6112 | 0.6129 | 0.6256 | 0.6073 |
| 37     | 0.5743                | 0.5797 | 0.5715 | 0.5564 | 0.5609 | 0.6164 | 0.6089 | 0.608  | 0.6082 |
| 38     | 0.5935                | 0.5988 | 0.5982 | 0.591  | 0.5887 | 0.6095 | 0.6168 | 0.601  | 0.6162 |
| 39     | 0.6435                | 0.6509 | 0.6538 | 0.6254 | 0.6238 | 0.6524 | 0.647  | 0.6403 | 0.6343 |
| 40     | 0.5926                | 0.6054 | 0.5973 | 0.575  | 0.5823 | 0.6096 | 0.5987 | 0.5951 | 0.5963 |
| 41     | 0.5917                | 0.5958 | 0.5837 | 0.571  | 0.5707 | 0.4746 | 0.4452 | 0.4839 | 0.4244 |
| 42     | 0.5171                | 0.5087 | 0.4728 | 0.4635 | 0.4275 | 0.5199 | 0.5134 | 0.5124 | 0.5094 |
| 43     | 0.5379                | 0.5414 | 0.545  | 0.5111 | 0.5038 | 0.5532 | 0.5405 | 0.5472 | 0.5184 |
| 44     | 0.5816                | 0.5748 | 0.5723 | 0.542  | 0.5456 | 0.565  | 0.5596 | 0.553  | 0.556  |
| 45     | 0.5776                | 0.5702 | 0.5653 | 0.5477 | 0.546  | 0.534  | 0.5363 | 0.5351 | 0.5421 |
| 46     | 0.5459                | 0.541  | 0.536  | 0.5129 | 0.5047 | 0.5452 | 0.5387 | 0.536  | 0.5356 |
| 47     | 0.5561                | 0.5377 | 0.5333 | 0.5171 | 0.5109 | 0.526  | 0.5147 | 0.5101 | 0.48   |
| 48     | 0.568                 | 0.5634 | 0.5564 | 0.5433 | 0.5373 | 0.5583 | 0.5472 | 0.55   | 0.5412 |
| 49     | 0.5782                | 0.5698 | 0.5583 | 0.5268 | 0.5118 | 0.61   | 0.5985 | 0.578  | 0.5739 |
| 50     | 0.6043                | 0.5968 | 0.5948 | 0.5814 | 0.5765 | 0.6085 | 0.6035 | 0.5769 | 0.596  |
| 51     | 0.6196                | 0.6084 | 0.6059 | 0.5847 | 0.5788 | 0.6039 | 0.5941 | 0.5845 | 0.5773 |
| 52     | 0.5285                | 0.5365 | 0.5364 | 0.5226 | 0.5078 | 0.5348 | 0.5253 | 0.5049 | 0.4859 |